

## TWO-BATH ELECTROLYSIS

### CROSS-REFERENCE TO RELATED APPLICATIONS

5           This application relates to US applications entitled: LIGHT SOURCE BODIES FOR FILAMENT TUBES AND ARC TUBES, Agent's Docket No. EF-101A; ONE PIECE FOLIATED LEADS FOR SEALING IN LIGHT SOURCES, Agent's Docket No. EF-101B; SPURRED LIGHT SOURCE LEAD WIRE FOR HANDLING AND FOR ASSEMBLING WITH A FILAMENT, Agent's Docket No. EF-101C; APPARATUS AND PROCESS FOR  
10   FINISHING LIGHT SOURCE FILAMENT TUBES AND ARC TUBES, Agent's Docket No. EF-101D and MOUNTING LIGHT SOURCE FILAMENT TUBES AND ARC TUBES IN LAMPS, Agent's Docket No. EF-101E; all having filing dates concurrent with that of the present invention.

### TECHNICAL FIELD OF THE INVENTION

15           The present invention relates to electric light sources and their manufacturing processes; and, more particularly, to said light sources in the form of a double ended, tipless filament tube or arc tube.

### BACKGROUND OF THE INVENTION

20           Although a variety of compact light sources are available, those with improved energy efficiency (lamp efficacy) are generally accompanied by proportionally higher manufacturing costs, and therefore by higher purchase prices that often outweigh their perceived benefit to ordinary consumers. For example, USP 4,524,302 (Berlec; 1985) discloses a general service incandescent lamp with improved efficiency having an outer envelope and an inner envelope. The inner envelope comprises what is generally known as a halogen lamp: a filament tube of  
25   quartz or high temperature glass, hermetically sealed around an incandescent filament, and filled with a relatively high pressure fill-gas including a halogen gas. Among the objects of this invention are to provide a relatively inexpensive general service incandescent lamp, to improve the arc-out resistance of the filament, and to operate at a low voltage so as to extend the life of the lamp while maintaining its wattage and even increasing its efficacy. The reduced voltages  
30   relative to a typical 120 volt AC source may be developed, for example, by an electrical transformer.

It is known that low voltage incandescent filaments are more rugged than higher voltage filaments having the same wattage, especially for coiled-wire filaments, because for any given wattage, as the design voltage is decreased the length of wire in the filament decreases, and the diameter of the wire in the filament increases. Two patents exemplify incandescent lamp designs that take advantage of this fact by providing multiple filament tubes that are series-connected within an outer envelope. This reduces the voltage drop across each filament tube without requiring a transformer, however the cost of the inner light source is multiplied by the number of filament tubes provided. USP 4,498,124 (Mayer et al.; 1985) discloses a dual halogen bulb rectangular lamp assembly with the two halogen bulbs electrically connected in series for simultaneous bulb energization. The use of two 12-volt halogen bulbs in a 24 volt reflector lamp significantly reduces the possibility of bulb burn-out because the filaments required in 12-volt halogen bulb units are made from shorter, thicker wire that can be coiled much more loosely than the filaments required in 24-volt halogen bulb units. PCT publication WO98/14733 (Katougi et al.; 1998) discloses a light bulb with a plurality of baseless small bulbs series-connected within a globe envelope, for improved earthquake resistance. Figure 8, for example, shows two double ended filament tubes with wire loop outer leads hanging in parallel arrangement on opposite sides of a central support post.

Another factor that adds to the cost of lamps that incorporate filament tubes (e.g., halogen lamps) is the desire to protect consumers from possible non-passive failure of the filament tube. When an incandescent filament fails at end of life, an electric arc may form between broken ends of the filament. Once started, an arc has very low electrical resistance and will draw as much current as the power supply allows. In arc lamps, the power supply includes some form of ballast to limit the current to a desired amount. Incandescent power supplies do not generally provide much ballasting effect, and rely instead on fuses and/or lamp construction to quench an end-of-life arc before it can produce violent failures that may, for example, rupture the filament-containing envelope(s) - i.e., to "explode". For filament tubes there is a small possibility of non-passive failure due to an arc that overheats the filament tube before the arc can be quenched by a fuse. A common solution is to make the outer lamp envelope out of a thick glass expected to contain a potentially rupturing inner envelope. For example, USP 6,133,676 (Chen; 2000) discloses a double enveloped halogen bulb wherein the outer glass envelope has a thickness ranging between 2 mm and 8 mm that is intended to protect a person or an animal contiguous to

the bulb from a bodily injury in the event that the tubular halogen bulb explodes. Chen's Figure 6 shows an embodiment of his outer envelope that is shaped somewhat like a common household light bulb. Obviously, the heavy glass envelope is much more expensive than a standard bulb.

Another solution for containing rupturing filament tubes is taught by related arc lamp art.

5 For lamps that incorporate arc tubes as the light source (e.g., high intensity discharge lamps), non-passive failure is even more of a concern, particularly when the light sources are intended for household use and/or wherever they will not be contained in protective "closed" lighting fixtures. USP 5,446,336 (Gleixner et al.; 1995) discloses an explosion-protected high-pressure discharge lamp comprising a protective body surrounding the discharge vessel and located within an outer  
10 bulb. The protective body comprises one or two transparent concentric glass sleeves or tubes, at least one of which, preferably, is of quartz glass. The sleeves or tubes have open ends, and they radially surround the discharge vessel, with the open ends being capped by ceramic centering and holding elements which are retained on a lamp holder structure.

A solution for preventing rupturing filament tubes is disclosed by the present inventor in  
15 the November/December 2001 issue of IEEE Industry Applications Magazine (incorporated by reference herein), wherein a mockup of a 1972 experimental "Gemini lamp" is pictured and described as having "small twin tubes paralleling the central glass stem – these low-pressure, 60-V halogen capsules would not explode.... [The] two small 60-V capsules [are] in series..." (pg.  
16). The pictured mockup has empty glass capsules, and the design of a filament for the capsule  
20 is not disclosed. Likewise, the capsule's shape is indeterminate, and no lead wires or sealing foils are present.

Figures 2, 4, and 5 of the Berlec '302 patent illustrate some common features of filament tubes. Figure 2 shows a typical quartz filament tube (22) with 1 mm thick walls that is double ended with an exhaust tube tip on the side of the tube. The tube ends are hermetically sealed by  
25 being pinched closed over a thin molybdenum foils (28, 32) that are micro-welded to inner (24c, 24e) and outer (30, 34) molybdenum lead wires. The inner lead wire may alternatively be tungsten, and is typically welded to the filament, however Figure 3 illustrates a technique of using the inner lead wire (24c, 24e) as a spud that is forced into the single coiled end (24b, 24d) of the filament (24). It is known that this spudding process is difficult to automate given that a  
30 blunt wire end must be screwed into the coil in a way that expands the coil diameter. Figure 4 illustrates a single ended filament tube (36) that is also made out of a high temperature glass

other than quartz. In this case, sealing can be accomplished on the round lead wires (38, 40) without needing foils. The illustrated filament tubes (22, 36) are relatively bulky and heavy, and therefore require substantial mounting structures (16, 18, 20, 42, 44, 46, 48) within the outer envelope (12). Figure 5 illustrates a somewhat smaller filament tube that is only suitable for very low voltage filaments that are consequently short enough to be mounted crosswise in the filament tube.

Several patents assigned to General Electric are indicative of the industry's efforts toward cost-reducing the manufacturing process for both filament tubes and arc tubes, particularly those small enough to be included in smaller lamps. USP 4,389,201 (Hansler and Fridrich; 1983),

incorporated by reference herein, discloses a method of manufacturing metal halide discharge lamps (arc tubes) on a horizontal glass blowing lathe which is indexed by a turntable through angularly spaced work stations. A length of quartz tubing is formed into a lamp body having an enlarged bulbous midportion defining an arc chamber with tubular necks projecting in opposite directions. Figures 9 and 10 show the bulbous midportion (32) being formed by heating (132) while longitudinally gathering the quartz (120) and then blowing it out into a mold (134).

Exhausting, flushing, and filling are all accomplished through the length of quartz tubing while it is captured in the lathe, thereby eliminating exhaust tube tips on the side of the arc tube. USP 4,810,932 (Ahlgren et al.; 1989), incorporated by reference herein, and other related patents adapt and enhance the '201 patented processes to disclose flush and pump flush processes

yielding light sources for both incandescent and metal vapor discharge lamps, particularly tipless double ended filament tubes that are suitable for deposition of a reflective coating on their outer surfaces. Figures 1(a)-1(p) show the flush process implemented in a horizontal lathe. Figure 1(d) shows the filament assembly (12) having a hook-shape section (12<sub>C</sub>) on one end and a loop extension section (12<sub>F</sub>) on the other for handling during the manufacturing process. Figure 1(f)

shows the filament assembly (12) being self-heated by the passage of electric current while flushing the surrounding tube (10) with an inert gas containing hydrogen. This step in the process removes oxygen contamination from within the confines of the light source body (10) and crystallizes the filament (12<sub>A</sub>) itself. By applying direct current to the filament positioned so that magnetic forces counter balance the force of gravity on the filament, the crystal structure of the filament may be set so that filament sag is avoided. Figure 1(h) shows the filament tube's midportion (10<sub>A</sub>) being blown into a mold (30) for precise dimensional control. Figures 1(m)

and 1(n) show liquid nitrogen (46) being used to condense a gas filling in the central portion (10a) while a torch (20) "shrink seals" the quartz body (10) around the foil sealing members (48, 50). The quartz shrinks without excessive heat because condensing the fill gas reduces the internal pressure of the body below atmospheric pressure. Figures 2(a)-2(l) and 3(a)-3(k) show the pump flush process implemented vertically for filament tubes and arc tubes, respectively. Minor differences from the horizontal flush process include straight ended lead wires handled by rods (72, 74) in an unspecified manner. Especially in the vertical process, the filament assembly (12) or electrodes (92) are held in place by first and second seal members abutting up against and respectively occupying the first and second neck portions of the tube body, such that bent edges of the foils (e.g., 12<sub>D</sub>, 12<sub>G</sub>) serve as springs to position and maintain the assembly (e.g., 12) on the central axis of the light source body. The seal members (12<sub>D</sub>, 12<sub>G</sub>, 92<sub>B</sub>, 94<sub>B</sub>) may be of the type described in USP 4,254,356 of Karikas, (further described hereinbelow). In preparation for mounting a finished filament tube or arc tube in an outer envelope, ends of the tube are removed by diamond saw cutting or scoring and snapping, thereby exposing a suitable length of the inlead wire extending beyond each end of the tube. As illustrated in Figures 6-10, the exposed lead wires are attached to a crossed lamp lead wire on at least one end, and where appropriate, to the base eyelet at the other end to provide a simplified mount structure.

USP 4,254,356 (Karikas; 1981), incorporated by reference herein, discloses inleads having a foil portion which is stiffened by reversely folded lateral edges, i.e., bent in opposite directions out of the medial plane. In making a discharge lamp, the electrode-inlead assembly is self-centering as a result of making the overall width of the foil portion and its reversely folded edges exceed slightly the internal diameter of the quartz tube or neck. The inlead assembly (1) comprises a one-piece molybdenum wire portion (2, 3) wherein the central portion (4) is foliated by longitudinal rolling to a thickness of about 0.0009" at the center. Karikas further teaches that the foliated portion (4) may also be produced by cross rolling and by swaging or hammering of the original wire, or may also use a composite foil comprising a cut length of molybdenum foil to one end of which is welded a molybdenum wire and to the other end a tungsten wire. No further details are provided about the proposed hammering process, and the present inventor is not aware of any practical mass production implementations of a foliation-by-hammering process in the lamp-making industry.

It is an overall object of the present invention to significantly reduce the manufacturing

cost of high-efficacy light sources, particularly those intended for household use, and more particularly those incorporating incandescent filament tubes contained within a protective outer envelope. Accordingly, it is an object to effectively eliminate the likelihood of non-passive failure for filament tubes in lamps made according to the invention. Accordingly, it is an object to mass-produce inexpensive filament tube envelopes. Accordingly, it is an object to mass-produce inexpensive foil/leadwire assemblies. Accordingly, it is an object to simplify leadwire-to-filament assembly and the handling of said assembly. Accordingly, it is an object to improve manufacturing efficiency for the flush-fill process. Accordingly, it is an object to improve the mounting of filament tubes within an outer envelope. Other subsidiary objects may become evident from the foregoing specification of the present invention.

A further object of the invention is to utilize suitable features of the inventive filament tubes in order to cost-reduce double ended arc tube lamp manufacturing.

#### BRIEF SUMMARY OF THE INVENTION

According to the invention, a method for electrolyzing a continuous length of metal is disclosed, the method comprising the steps of: firstly passing the length of metal through electrolysis fluid contained in a first bath that also contains a first electrode connected to a first pole of a power supply; secondly passing the length of metal through electrolysis fluid contained in a second bath that also contains a second electrode connected to a second pole, opposite to the first pole, of the power supply; and using the length of metal as an electrical conductor for completing the electrical circuit between the electrolysis fluid of the first bath and the electrolysis fluid of the second bath.

According to the invention, the method further comprises the step of passing the length of metal through the first bath and through the second bath by passing through a plurality of seals below a fluid level of the electrolysis fluid such that each one of the plurality of seals allows passage of the length of metal while limiting fluid loss. Preferably the method further comprises the step of cooling the length of metal by providing a one of the plurality of seals such that the one seal maintains immersion of the length of metal in electrolysis fluid while the length of metal passes from the first bath to the second bath.

According to the invention, the method is such that the power supply is an AC power supply.

According to the invention, the method further comprises the step of moving the length of

metal in one direction through the first bath and through the second bath.

According to the invention, a two-bath electrolysis line for performing electrolysis on a continuous length of metal is disclosed, the electrolysis line comprising: a first bath containing electrolysis fluid filled to a fluid level, and a first electrode, the first electrode being connected to a first pole of a power supply; a second bath containing electrolysis fluid filled to a fluid level, and a second electrode, the second electrode being connected to a second pole, opposite to the first pole, of the power supply; a conveyance path such that the length of metal passes first through the electrolysis fluid in the first bath, and second through the electrolysis fluid in the second bath; and a conductor of electrical current between the electrolysis fluid in the first bath and the electrolysis fluid in the second bath, the conductor being the length of metal.

According to the invention, the electrolysis line further comprises a plurality of seals that allow passage of the length of metal through the first bath and through the second bath below the fluid level of the electrolysis fluid while limiting fluid loss. Preferably the plurality of seals comprises a plurality of grommet seals that are mounted within holes below the fluid level of the electrolysis fluid in each of the first bath and second bath, the holes being located in opposed ends of the first bath and in opposed ends of the second bath. Preferably a one of the plurality of grommet seals connects the first bath to the second bath. Preferably an end of the first bath abuts an end of the second bath; and the one of the plurality of grommet seals is mounted within holes through the abutting ends.

According to the invention, the electrolysis line is such that the power supply is an AC power supply.

According to the invention, the electrolysis line further comprises an advancing device that moves the length of metal through the first and second baths.

Other objects, features and advantages of the invention will become apparent in light of the following description thereof.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Reference will be made in detail to preferred embodiments of the invention, examples of which are illustrated in the accompanying drawing figures. The figures are intended to be illustrative, not limiting. Although the invention is generally described in the context of these preferred embodiments, it should be understood that it is not intended to limit the spirit and scope of the invention to these particular embodiments.

Certain elements in selected ones of the drawings may be illustrated not-to-scale, for illustrative clarity. The cross-sectional views, if any, presented herein may be in the form of "slices", or "near-sighted" cross-sectional views, omitting certain background lines which would otherwise be visible in a true cross-sectional view, for illustrative clarity.

5 Elements of the figures can be numbered such that similar (including identical) elements may be referred to with similar numbers in a single drawing. For example, each of a plurality of elements collectively referred to as 199 may be referred to individually as 199a, 199b, 199c, etc. Alternatively, a single element (e.g., shaft 391) may have multiple parts (e.g., shaft inside end 391a, shaft outside end 391b). Or, related but modified elements may have the same number but  
10 are distinguished by primes. For example, 109, 109', and 109'' are three different elements which are similar or related in some way, but have significant modifications, e.g., a tire 109 having a static imbalance versus a different tire 109' of the same design, but having a couple imbalance. Such relationships, if any, between similar elements in the same or different figures will become apparent throughout the specification, including, if applicable, in the claims and abstract.

15 The structure, operation, and advantages of the present preferred embodiment of the invention will become further apparent upon consideration of the following description taken in conjunction with the accompanying drawings, wherein:

Figure 1A is a filament tube light source assembly in process, according to the prior art;

Figure 1B is a lamp assembly, according to the prior art;

20 Figures 2A-2E illustrate a process for manufacturing double ended, tipless bodies for light sources as practiced on a lathe, according to the invention;

Figure 2A is a side view of a working end of tubing stock in the lathe, according to the invention;

25 Figure 2B is a side view of the tubing being heated by a shaped burner, according to the invention;

Figure 2C is a side view of a necked-in portion of the tubing being heated by a narrow-flame burner, according to the invention;

Figure 2D is a side view of a cusped maria formed in the necked-in portion of the tubing, according to the invention;

30 Figure 2E is a side view of a completed body cut off of a remaining portion working end of the tubing, according to the invention;



Figure 2F is a side view of two completed bodies cut off of a remaining portion working end of the tubing, made by alternate process embodiments according to the invention;

Figure 3 is a side view of a lead processing line for implementing a foliated lead manufacturing process, according to the invention;

5        Figure 4A is a cross-sectional view, taken along the line 4A-4A of Figure 3, of a wire that is positioned between working faces of hammers for foliating the wire in a hammering stage of the foliated lead manufacturing process, according to the invention;

10        Figure 4B is a cross-sectional view, taken along the line 5B-5B of Figure 5A, shading omitted for clarity, of idealized (flattened) profiles of the wire as it progresses from an un-hammered wire down to an N-blow foil in the hammering stage of the foliated lead manufacturing process, according to the invention;

Figure 5A is a top view of a foil resulting from the hammering stage of the foliated lead manufacturing process, according to the invention;

15        Figure 5B is a cross-sectional view, taken along the line 5B-5B of Figure 5A, of the foil resulting from the hammering stage of the foliated lead manufacturing process, according to the invention;

Figure 6A is a top view of a straightened foil resulting from a foil straightening process of the foliated lead manufacturing process, according to the invention;

20        Figure 6B is a cross-sectional view, taken along the line 6B-6B of Figure 6A; of the straightened foil resulting from the foil straightening process of the foliated lead manufacturing process, according to the invention;

Figure 7A is a top view of wire, foliated according to the invention, that is passing through first and second etching baths in a foil etching stage of the foliated lead manufacturing process, according to the invention;

25        Figure 7B is an end view of a grommet seal for allowing passage of the foliated wire through the etching baths of Figure 7A, according to the invention;

Figure 8A is a perspective view of a wire cutter, according to the invention;

Figure 8B is a side view of a portion of wire having a straight cut end with double-sided spurs resulting from a cutting process, according to the invention;

30        Figure 8C is an edge view of a straight or angled cut end resulting from the cutting process, according to the invention;

Figure 8D is a side view of a portion of wire having an angled cut end with a one-sided spur resulting from the cutting process, according to the invention;

Figure 8E is a top view of a one-piece foliated lead that results from a preferred embodiment of the lead manufacturing process implemented on the lead processing line of Figure 3, according to the invention;

Figures 9A-9C illustrate a process for manufacturing light source filament assemblies, according to the invention;

Figure 9A is a side view of a primary coil comprising a filament wire that is wound on a primary mandrel, according to the invention;

Figure 9B is a side view of a coiled coil filament being assembled with first and second foliated leads (portions visible), according to the invention;

Figure 9C, is a full side view of a completed filament assembly, according to the invention;

Figures 10A-12C and Figures 15A-15B illustrate preferred embodiments of a light source finishing process for manufacturing light sources, according to the invention;

Figure 10A is a cross-sectional view of a finishing head, with the filament assembly of Figure 9C (not cross-sectioned) held in a collet of the finishing head, and with clamshells hingedly opened downward, according to the invention;

Figure 10B is a cross-sectional view of a finishing stand comprising the colleted top finishing head of Figure 10A holding the filament assembly of Figure 9C (not cross-sectioned), and a colletless bottom finishing head, with the light source body (not shaded) of Figure 2E sealingly held by closed clamshells of both finishing heads, according to the invention;

Figure 10C is a view of the finishing stand of Figure 10B illustrating a step of the light source finishing process comprising making a first seal of the body around a foliated lead of the filament assembly, according to the invention;

Figure 10D is a view of the finishing stand of Figure 10B illustrating a step of the light source finishing process comprising freezing fill gas into the body and making a second seal of the body around a foliated lead of the filament assembly, according to the invention;

Figure 10E is a side, foil-edge view of a finished filament tube light source, according to the invention;

Figure 10F is a side view, rotated 90° from the view of Figure 10E, of a finished filament

tube light source, according to the invention;

Figure 11A is a top view of the collet of the colleted finishing head of Figure 10A, according to the invention;

5 Figure 11B is a cross-sectional view, taken along the line 11B-11B of Figure 11A, of the collet of Figures 10A and 11A, showing portions of the finishing head in which the collet is mounted, according to the invention;

Figure 11C is a top view of clamshells hingedly connected to a frame, according to the invention;

10 Figure 12A is a cross-sectional view of a bugled end of a light source body (not shaded) being loaded into a finishing head for which relevant portions are shown including an inner tube and clamshells, according to the invention;

Figure 12B is the finishing head portions and bugled end of Figure 12A showing the bugled end being laterally centered by interacting with the inner tube, according to the invention;

15 Figure 12C is the finishing head portions and bugled end of Figure 12B showing the bugled end being coaxially aligned with the inner tube by the closed clamshells, according to the invention;

Figure 13A is a side view of an embodiment of a lamp wherein two filament tube light sources are mounted in a general service incandescent lamp, according to the invention;

20 Figure 13B is a side view, with an outer envelope shown in cross-section, of an embodiment of a lamp wherein one arc tube light source is mounted in a sealed beam headlamp, according to the invention;

Figure 14 is a side view, with body material shown in cross-section, of a bugled end of a light source body illustrating an electrical support connection to an outer lead wire of the light source, according to the invention;

25 Figure 15A is a cross-sectional view of a finishing stand comprising a colleted top finishing head holding a first electrode assembly (not cross-sectioned), and a colleted bottom finishing head holding a second electrode assembly (not cross-sectioned), with the light source body (not shaded) of Figure 2E sealingly held by closed clamshells of both finishing heads, according to the invention; and

30 Figure 15B is a side view of a finished arc tube light source, according to the invention.

#### DETAILED DESCRIPTION OF THE INVENTION

The present invention, described hereinbelow in preferred embodiments, comprises manufacturing process steps that improve upon prior art processes for the manufacturing of light sources (both filament tube and arc tube), and lamps employing said light sources, generally by mounting the light source within an outer envelope of a lamp. The improved manufacturing process steps result in improved subassemblies, improved light sources, and improved lamps, all of which are therefore intended to be within the scope of the herein-disclosed invention(s). Many of the inventive improvements are directed toward cost-reducing light source production, especially for lamps that comprise one or preferably two light sources mounted in an outer envelope. In particular, the cost-reduced improved processes can be utilized in the manufacturing of a lamp such as the Gemini lamp wherein two filament tubes are mounted in an outer envelope to form a lamp that is affordable for common household consumer usage as a result of the inventive cost reduced manufacturing processes.

The preferred embodiments are described primarily for "filament tube" type light sources that use an incandescent tungsten filament, generally coiled, and mounted within a tubular quartz (fused silica) envelope (light source body) to form a tipless double ended filament tube. More particularly, the preferred embodiment light source is a 60 volt, 50 watt halogen filament tube for mounting two-in-series in a lamp outer envelope (e.g., lamp 400 in Figure 13A) thereby creating a 100W, 120V halogen lamp. The quartz tube is hermetically sealed around the filament by means of the well known technique of using a thin molybdenum foil as the electrical conductor passing through each seal area (the hermetic seal). Many of the same components and processes can be extended for use in the manufacturing of double ended, tipless "arc tube" type light sources (e.g., metal vapor discharge lamps), and all such alternate embodiments - some examples of which are herein illustrated and described - are intended to be within the scope of the present invention. The term "light source" is therefore intended to encompass any electrically-powered source of radiation (e.g., visible, infrared, etc.) that is manufacturable according to the present invention, particularly for incandescent filament light sources generally known as filament tubes, and for arc-between-electrodes light sources generally known as arc tubes. Furthermore, herein-disclosed processes may have other applications, which are also intended to be within the scope of the present invention. For example, the foliated wire and it's manufacturing process could be used in other types of quartz sealing applications. For example, the light source bodies could be manufactured according to the inventive process as adapted to form glass or other non-quartz

vitreous material that can be, for example, sealed around wires instead of the described foliated lead wires. Accordingly; the terms quartz and glass may be used herein interchangeably, and are intended to be exemplary embodiments of a broader class of vitreous materials, particularly those that are suitable for light source manufacturing.

5           As detailed in the background hereinabove, the prior art contains many examples of light sources comprising either filament tubes or arc tubes that are housed in an outer envelope to form a complete lamp. Furthermore, various manufacturing processes for such lamps are described, e.g., by the Ahlgren '932 patent. By way of reference, Figures 1A and 1B show prior art filament tube and lamp assemblies, e.g., as described in the Ahlgren '932 patent (part numbering  
10   modified). Figure 1A shows a hollow tubular light source body 1010 held in a head 1016 of a horizontal glass lathe for further processing. A filament assembly 1012 is provided having a filament 1012A with predetermined voltage characteristics, a first lead 1012B having one of its ends 1110 with attachment means shown as a hook-shape section 1012C and its other end connected to a first foliated seal member 1012D which is further connected to one end of the  
15   filament 1012A. A second lead 1012E having one end 1112 with attachment means shown as a loop extension section 1012F and its other end connected to a second foliated seal member 1012G which, in turn, is further connected to the other end of the filament 1012A. Subsequent processing yields a finished filament tube light source 1100 that is shown in Figure 1B as being mounted in a type of lamp that is a sealed beam headlamp 1170. The sealed beam headlamp  
20   1170 has a reflector 1172 and lens 1173 and a pair of ferrules 1174 and 1176 located at the base of the reflector 1172. The ferrules 1174 and 1176 are respectively connected to a pair of electrical terminals 1178 and 1180. The filament 1012A of the light source 1100 is connected across the pair of ferrules by first 1182 and second 1184 electrical support wires that are electrically and mechanically connected to the first and second lead ends 1110 and 1112,  
25   respectively. During filament tube processing, the attachment means 1012C, 1012F have been cut off, and the body 1010 has been formed as shown in Figure 1B. In particular, the filament 1012A is centered in a blown-out portion 1118, and the body 1010 has been sealed 1102, 1104 about the first and second seal members 1012D, 1012G, respectively, wherein the sealing process is completed after pumping, flushing, and filling the light source body 1010 with a suitable light  
30   source ingredient. The processing of the light source is accomplished through the legs 1106, 1108 of the body 1010, thereby obviating the need for an extra exhaust tube and its tip-off. The

prior art also discloses similarly-manufactured light sources that employ opposed arc electrodes in place of the filament 1012A, thereby creating an arc tube type of light source that can be similarly mounted in an outer envelope such as the reflector 1172 and lens 1173 to form a lamp.

### **Light Source Body Manufacturing**

5        Figures 2A-2E show an improved process for manufacturing double ended, tipless bodies (e.g., body 22 in Figure 2E) for light sources (e.g., filament tubes, arc tubes). This process can be practiced on any suitable glass lathe, and is preferably automated to both minimize manufacturing cost, and to provide dimensional consistency from part to part. Furthermore, one or more of the suitable glass lathes can be incorporated as a portion of an assembly line,  
10        preferably automated, that makes light sources and lamps according to the invention. The described embodiment of the body manufacturing process is illustrated with a horizontal glass lathe, although the horizontal orientation is not intended to be limiting. However, it may be noted that making an end-to-end symmetric bulb would more difficult on a vertical lathe due to unsymmetrical heat loss. The inventive body manufacturing process will be seen to be a cycle  
15        that proceeds in order through steps illustrated by Figure 2A, followed by Figure 2B, etc., through Figure 2E which is then cyclically followed by the step of Figure 2A, and so on - thereby sequentially manufacturing multiple light source bodies 22 from a single length of tubing stock material. Figures 2A-2E illustrate lathe-formed tubing in profile wherein it should be understood that the profile shapes (including contours and dimensions) are rotationally equivalent about a  
20        longitudinal axis of the tubing.

      Figure 2A shows a headstock 6 of a glass lathe 4 (only relevant portions of the lathe 4 are illustrated as needed in Figures 2A-2E). The collet of the headstock 6 is laterally and longitudinally fixed, but rotates at predetermined speeds as required. The headstock collet 6 grips a length of hollow tubular vitreous material, e.g., 3x5 mm quartz tubing 10 (nominally 3  
25        millimeter inside diameter, 5 millimeter outside diameter D1, and thus a 1 millimeter wall thickness T1). Since multiple light source bodies 22 are to be formed from a single length of tubing 10, the lathe 4 is adapted to accommodate a suitable length dimension for a supply end 10b of the tubing 10 extending to the right of the headstock 6. To the left of the headstock 6 a working end 10a of the tubing 10 extends. In Figure 2A the working end 10a has been  
30        previously worked such that it comprises a transitional portion 12, a necked-in portion 14, and a bugled end 16. The illustration of Figure 2A assumes that the working end 10a is the result of

completing the step illustrated by Figure 2E and removing a light source body 22 completed in that step. It should be obvious that in the case of starting with a new length of tubing 10, the steps of Figures 2B-2E must be carried out on a working end 10a that does not have a transitional portion 12, a necked-in portion 14, and a bugled end 16, in order to create these requisite portions for the next implementation of the step of Figure 2A. Also obviously, the body resulting from this first process cycle will be undesirably single-ended, and is generally scrapped, although as an alternative it could be turned around and joined to the non-bugled working end 10a of another new length of tubing 10. A tailstock collet 8 (see Figure 2B) will obviously need to be able to accommodate the diameter of the tubing 10 as well as the diameter of the necked-in portion 14. It is also advantageous to use collet jaws that have, for example, swivel pads in order to accommodate tapered and/or skewed tubing profiles.

Figure 2B shows a step wherein a tailstock collet 8 of the lathe 4 has gripped the necked-in portion 14 of the working end 10a and pulled it through a loosened headstock collet 6 to stop the bugled end 16 at a first predetermined position 21a, whereupon the headstock collet 6 is retightened, and the lathe 4 (by means of the headstock 6 and tailstock 8) begins rotation of the tubing 10 at a predetermined rotational speed. A shaped burner 26 is positioned at a first burner position 23a such that heat (e.g., from a flame 28) is applied to the working end 10a of the tubing 10. The first burner position 23a is selected to produce a body 22 of a desired overall length L (referring to Figure 2E). The flame 28 is preferably shaped by the shaped burner 26 to vary the amount of heat produced by different portions of the flame 28, thereby heating the tubing 10 in a way that varies along the length of the tubing 10 in a predetermined pattern (shape). The shape of the flame 28 may continuously vary, but a simple example of flame shaping is presented in Figure 2B wherein the flame 28 has a central low heat zone 28b that is symmetrically bookended by two higher heat zones 28a, 28c. Immediately after the flame 28 has heated the tubing 10 to a predetermined temperature above its softening point, the tailstock 8 is biased with a controlled amount of a bias force F1 directed to the left, thereby placing the tubing 10 in tension. In its simplest form, the bias force F1 can be applied with a weight on cable and pulley arrangement. A more sophisticated method comprises, for example, a stepper motor with force limiting controlled to start stretching the tubing 10 at the appropriate time. Preferably some form of controller 5 is provided to control force, timing, rate, and extent of the stretching induced in the heated region of the tubing 10. The controller 5 (e.g., a programmable controller 5 associated

with the lathe 4) preferably also controls timing and positioning of the shaped burner 26 such that the flame 28 is turned on and off, optionally varied in heat output and optionally controlled separately in its heat zones 28a, 28b, 28c. Further preferably, the shaped burner 26 is moved left in concert with the leftward movement of the bugled end 16, thereby constantly maintaining heat in the center of a stretched-out (and therefore necked-in) portion 14' of the tubing 10 (refer to Figure 2C). Alternatively, the headstock 6 and tailstock 8 may be moved equal distances at the same rate in opposite directions. This, of course, requires a lathe with a longitudinally moveable headstock.

Figure 2C shows a step that starts with the working end 10a that has been shaped by the process of the previous step of Figure 2B. Preferably the lathe is still rotating the tubing 10 at a predetermined speed. Under the influence of the bias force F1, the tubing 10 that was heated by the shaped burner 26 has been stretched to form the stretched-out portion 14' bookended by a left transitional portion 12a and a right transitional portion 12b. A bulb 18 portion of the tubing 10, with the original straight-sided outside diameter D1 and wall thickness T1, remains between the left transitional portion 12a and a previous transitional portion 12c (12 in Figure 2A that was formed in a previous process cycle). The flame heat zones 28a, 28b, 28c of the shaped burner 26 have been adjusted to create a smooth contour for the transitional portions 12a, 12b, and movement of the shaped burner 26 can assure that the left transitional portion 12a has substantially the same contour as the right transitional portion 12b. It should be noted that the contour of the transitional portions 12a, 12b not only longitudinally varies smoothly in outside diameter, but optionally also longitudinally varies smoothly in wall thickness. Smooth variation is herein defined to include a monotonic variation from a first dimension to a second, different dimension. With suitable process control, the transitional portions 12a, 12b will smoothly transition between the tubing 10 outside diameter D1 and a smaller predetermined necked-in diameter D2; similarly the tubing 10 wall will smoothly transition between a tubing 10 wall thickness T1 and a predetermined necked-in wall thickness T2 that is optionally smaller than the tubing wall thickness T1. Preferably a necked-in portion inside diameter ( $D2 - 2 \cdot T2$ ) is approximately equal to, or slightly larger than a foil width Wf for a sealing foil (e.g., foil 76 in Figure 6B). It should also be noted that the controller 5 provides control that is consistent, precise and repeatable from cycle to cycle such that the shape and dimensions of the previous transitional portion 12c are substantially duplicated or mirrored by the shape and dimensions of



the left transitional portion 12a and the right transitional portion 12b. The step of Figure 2C proceeds such that a first cooling time is allowed after removal of heat from the shaped burner 26 (e.g., the shaped burner 26 is moved away from the tubing 10). The first cooling time is sufficient to allow the tubing 10 to cool at least below its glass transition temperature. After completion of the first cooling time, a narrow-flame burner 30 is positioned at a second burner position 23b selected such that heating from a flame 32 of the narrow-flame burner 30 is applied to a relatively narrow cylindrical band 24 of the rotating tubing 10, the band 24 being located at a longitudinal center of the stretched-out portion 14' (i.e., at the second burner position 23b). As soon as the tubing 10 in at least the longitudinal center 23b of the cylindrical band 24 becomes plastic, the narrow-flame burner 30 is turned off and/or removed and a longitudinal compressive force F2 is applied to the working end 10a (e.g., the tailstock 8 is forced to the right) while the tubing 10 cools down through the glass transition temperature.

Figure 2D shows a step that starts with the working end 10a that has been shaped by the process of the previous step of Figure 2C. The compressive force F2 has been applied (e.g., by a spring, not shown) in a way that relatively quickly moved a previous bugled end 16c (an instance of the bugled end 16 shown in Figures 2A, 2B, 2C) from the second predetermined position 21b to a third predetermined position 21c. It is known in the glass working arts that longitudinal compression applied to a heated tube will produce a bulged-out region commonly called a "maria". If the compressive force is applied after the glass becomes plastic and continued while the glass cools down through the glass transition temperature, the center of the maria (where the glass is hottest) will bulge out the most and is likely to form a sharply cusped contour where the cooler and therefore stiffer glass on the left of the maria's center essentially tangentially joins the cooler glass on the right of the center. A maria that is cusped this way would normally be considered defective because it is very fragile, i.e., liable to easily crack along the cusp. According to the present invention, a relatively high longitudinal compressive force F2 is applied to the working end 10a until after the heated band 24 of tubing 10 cools below the glass transition temperature such that a cusped maria 20 is intentionally formed comprising a cusp 19 (providing a fragile ring around the center of the stretched-out portion 14' of the working end 10a), and on either side of the cusp 19 providing left and right bugled ends 16b, 16c, respectively. Each bugled end 16 comprises an end for the tubing 10 that is flared out diametrically and has a rotationally symmetric profile similar to that of the bell of a bugle. After

forming the cusped maria 20, the lathe 4 continues to rotate until the tubing 10 has cooled at least below the glass transition temperature, whereupon the lathe 4 stops rotating. Either just before, or soon after the lathe 4 stops rotating, the cusp 19 is caused to break by placing it in tension (a longitudinal break-off force F3), optionally assisted by tapping on the headstock collet 6 with a hammer 2, thereby initiating a mild shock wave that will cause a ring-off type of crack to occur along the line of the fragile cusp 19.

Figure 2E shows a step that starts after the completion of the process of the previous step of Figure 2D. The lathe 4 is no longer rotating, and the tailstock 8 has been moved to the left after the cusped maria 20 has been wrung-off. As a result, the working end 10a of the previous step (illustrated in Figure 2D) has been separated into a completed body 22 and a remaining portion working end 10a'. Preferably the lathe controller 5 has controlled the formation of the cusped maria 20 such that the formation is repeatable from cycle to cycle, thus forming duplicate (identical though mirrored) shapes at both ends of each body 22 as well as substantially duplicate overall shapes from body 22 to body 22. In other words, the previous transitional portion 12c is substantially duplicated or mirrored by the shape and dimensions of the left transitional portion 12a and the right transitional portion 12b; the previous necked-in portion 14c is substantially duplicated or mirrored by the shape and dimensions of the left necked-in portion 14a and the right necked-in portion 14b; and the previous bugled end 16c is substantially duplicated or mirrored by the shape and dimensions of the left bugled end 16a and the right bugled end 16b. In terms of dimensions, outside diameters D1, D2 and wall thicknesses T1, T2 (defined hereinabove) are controlled to be substantially duplicated in every relevant portion of every body 22 produced according to the present invention. Length dimensions, measured longitudinally along the tubing 10 and body 22, are illustrated in Figure 2E and should likewise be understood to be controlled so as to be substantially duplicated in every relevant portion of every body 22 produced according to the present invention. The body 22 has a body length L that is subdivided into two bugled end lengths LB1, LB2; two necked-in portion lengths LN1, LN2; two transitional portion lengths LT1, LT2; and one bulb length LB. The corresponding lengths in the remaining portion working end 10a' have a right bugled end length LB3; a right necked-in portion length LN3; and a right transitional portion length LT3. Suitable control by the controller 5 will cause the bugled end lengths to be substantially equal to each other ( $LB1 = LB2 = LB3$ ); the necked-in portion lengths to be substantially equal to each other ( $LN1 = LN2 = LN3$ ); and the transitional

portion lengths to be substantially equal to each other ( $LT1 = LT2 = LT3$ ). Similarly, the body length  $L$  and the bulb length  $LB$  will be substantially equal to their corresponding lengths in all bodies 22 made according to the present invention.

To complete the step of Figure 2E, the tailstock collet 8 is opened and the body 22 is removed for further light source assembly processes. For example, the body 22 could be ejected or otherwise caused to fall into an accumulation tray (not shown). For example, a mechanical transfer could grip the body 22, remove it from the tailstock 8, and transfer the body 22 for further processing. Following removal of the body 22, the process cyclically proceeds to the step of Figure 2A, wherein the remaining portion working end 10a' becomes the new working end 10a for the process step of Figure 2A. Similarly, the right bugled end 16b, the right necked-in portion 14b, and the right transitional portion 12b become the new bugled end 16, necked-in portion 14, and transitional portion 12, respectively.

It can be seen that the light source body 22 formed by the above-described inventive process is a tipless double ended body formed without the complication and expense of blowing out into a mold or using a cutoff saw/torch/laser/etcetera. As will be seen in the description hereinbelow, the bugled ends 16a, 16c (collectively referred to as 16) not only provide a simple means of cutoff, but also provide advantages in a finishing (e.g., flush/fill) process and in mounting of the light source in a lamp. The bulb portion 18 can be of any desired bulb length  $LB$ , including the limiting case wherein the transitional portions 12a, 12c (collectively referred to as 12) adjoin each other causing a straight sided bulb length  $LB$  of zero, thereby forming a smoothly rounded center for the body 22 similar to mold-blown bulb contours of the prior art. Such a body 22 with a rounded center may be desired for a small arc tube, for example. If the body 22 is formed with the optional variation in wall thickness (see Figure 2C), then several possible advantages ensue. Less tubing 10 is utilized in each body 22. The necked-in portions 14a, 14c (collectively referred to as 14) will be less massive, and therefore will store less heat in an operating light source. In a filament tube wherein an incandescent filament is mounted in the body 22 (as described hereinbelow), the transitional portions 12 can be shaped, thinned, and positioned relative to the ends of the filament such that the body 22 is substantially isothermal at least around the enclosed volume of the light source during operation of the filament tube light source.

A further advantage of the inventive bugled ends 16 is the ability to use them for making

a simple connection to a blow pipe in manufacturing processes wherein it is desired to blow out the bulb 18 (e.g., blowing into a mold). As shown, for example, in Figure 12B, a relatively airtight connection between a tube (e.g., tube 170) and the bugled end 16 can be made simply by pushing the tube (e.g., 170) into the bugled end 16, even if the tube (e.g., 170) is slightly off-axis relative to the body 22. Furthermore, a cut off single-bugled working end 10a could be turned around and joined to the non-bugled working end 10a of a new length of tubing 10, thereby providing a bugled end 16 for making a blowing connection for the first body 22 being formed at the working end of a new length of tubing 10.

Figure 2F illustrates several features of light source bodies produced by possible alternate embodiments of the present inventive process. A first alternate body 922a and a second alternate body 922b (produced in sequence after the first alternate body 922a) are shown after being cut off to leave a remaining portion working end 910a' that is still held by the headstock 6 of the lathe 4.

Two different cutoff methods are used in alternating sequence for successive alternate bodies 922a, 922b. The cusped maria process, described hereinabove, has been used to create left and right alternate bugled ends 916a, 916b where the first alternate body 922a has been cut apart from the second alternate body 922b in a second cutoff 915b. However, a first cutoff 915a and a third cutoff 915c were made using a method other than the inventive cusped maria process (a non-maria cutoff method) to create non-bugled ends 917, collectively referring to a previous non-bugled end 917c at the first cutoff 915a, plus a left non-bugled end 917a and a right non-bugled end 917b at the third cutoff 915c. The non-maria cutoff method used for the alternate embodiment illustrated in Figure 2F can be, for example, a known method employing a cutoff saw. By alternating cutoff methods, it can be seen that each of the alternate bodies 922a, 922b will have one bugled end (e.g., 916a or 916b) and one non-bugled end (e.g., 917c or 917a).

Figure 2F also illustrates another simplification of the inventive process whereby the necked-in portions (e.g., 14a, 14c for the body 22 in Figure 2E) are omitted from the body manufacturing process. For example, the first alternate body 922a has an alternate bulb 918 longitudinally centered in the overall body length L, having a bulb length LB and a bulb diameter equal to the tubing outside diameter D1. The alternate bulb 918 is bookended by diametrically opposed tubular portions: a left tubular portion 914a having a left tubular portion length LL1 and a left tubular portion diameter equal to the tubing outside diameter D1; and a right tubular portion 914b having a right tubular portion length LL2 and a right tubular portion diameter equal

to the tubing outside diameter D1 (except for the bugled end 916a). The tubular portions 914a, 914b in this example have equal lengths (i.e.,  $LL1 = LL2$ ). Later light source manufacturing steps include sealing the tubular portions 914a, 914b around lead wires and it should be noted that shrink sealing, for example, will neck in part of each tubular portion 914a, 914b, thereby further defining the shape and dimensions of the alternate bulb 918.

### **Lead Manufacturing**

Figures 3-8E show an improved process for manufacturing one piece foliated leads (e.g., foliated lead 74 in Figure 8E) for sealing in light sources (e.g., filament tubes, arc tubes). This process is preferably automated (e.g., using a lead processing line 40 as shown in Figure 3) to both minimize manufacturing cost, and to provide dimensional consistency from part to part. Furthermore, one or more of the lead processing lines 40 can be incorporated as a portion of an assembly line, preferably automated, that makes light sources and lamps according to the invention.

Figure 3 shows a preferred embodiment of the inventive lead manufacturing process, exemplified by the lead processing line 40, which has several inventive features as detailed in Figures 4A-8E, described hereinbelow. The lead processing line 40 starts on the left with a wire supply spool 44 of wire 42, processes the wire 42 into a foliated wire 43 by creating a spaced string of foils 76, and then finishes on the right by sequentially cutting completed one piece foliated leads 74 off the end of the foliated wire 43 (for convenience in the foregoing discussion, the terms "wire 42", and "foliated wire 43" may be used interchangeably and each term should be understood to include the other term where logically appropriate since both terms refer to the same wire 42 being processed and advanced through the lead manufacturing process). The wire 42 is preferably molybdenum wire suitable for sealing and having the same diameter (e.g., 0.007") as a primary mandrel (e.g., 106 in Figure 9A) for a filament (e.g., 102 in Figure 9B) of the filament tube type of light source that will be made using the foliated lead 74. Alternatively for arc tube light sources, the wire 42 is molybdenum wire that is suitable for sealing and for making into an arc electrode (e.g., first and second electrodes 306, 308 in Figure 15A). Further alternatively for arc tube light sources, the electrode (e.g., 306, 308) can be separately made (e.g., from tungsten wires), and subsequently attached (e.g., butt welded) to the foliated lead 74 that is produced by the lead manufacturing process described herein.

The spool 44 incorporates suitable tensioning devices (e.g., spool brake 45) and wire

guiding capabilities (not shown). The wire 42 is advanced through the lead processing line 40 by a wire advancing device embodied here as an advancing gripper 56 combined with a stationary gripper 58 such that the foliated wire 43 is held by the stationary gripper 58 while the advancing gripper 56 with open jaws moves to the left, and the foliated wire 43 is advanced to the right by the advancing gripper 56 with closed jaws while the stationary gripper 58 has open jaws. The advancing gripper 56 (e.g., under control of a stepper system) is also used in combination with the spool brake 45 to function as a tensioning device that provides tension and movement for accommodating elongation of the wire 42 as described hereinbelow. The grippers 56, 58 have jaw shapes, and are positioned, such that the foils 76 are not damaged by the gripping and advancing operations (e.g., the foils 76 are never touched by the grippers 56, 58).

The lead processing line 40 produces a new foliated lead 74 every cycle, wherein the machine cycle comprises: advancing the wire 42, and processing portions of the wire 42 simultaneously in each of several stages of the lead manufacturing process. The wire 42 is advanced by a "step" distance selected to produce a uniform desired foil spacing FS (see Figure 7A). It will be seen that the selected amount of initial advancement is slightly less than the foil spacing FS in order to accommodate elongation of the wire 42 that occurs in some of the stages. Thus during each machine cycle the wire 42 is advanced one step equaling the foil spacing FS, but comprised of an initial advancement distance plus the small amount of elongation that occurs during the cycle. The machine cycle timing (per completed foliated lead 74) is determined by the most time-consuming stage of operation, that being a hammering stage that has been proven at a rate of at least 90 per minute, i.e., a cycle time of 0.67 seconds. The stages of the lead manufacturing process will now be presented in sequential order.

Referring to Figures 3, 4A and 4B, a first stage of the lead manufacturing process is foil hammering wherein a portion of the wire 42 is hammered into a thin, sharp-edged sealing foil between a top hammer 46a and a bottom hammer 46b driven by a hammering drive 47. The hammers 46a, 46b (collectively referred to as hammers 46) are cemented carbide and have identically shaped working surfaces: a working face 92 on a truncated conical frustum 90. The working face 92 has a slightly convex surface centered on an axis of revolution AR, and is rounded at an edge 94 where it transitions to the frustum 90. For example, the working face 92 has an oblate spheroid surface with a major-to-minor axis ratio of about 100 to 1, wherein an axis of revolution AR lies along the minor axis of the oblate spheroid, and the rounded transition edge

94 ends at the frustum 90 along the major axis of the oblate spheroid. The hammers 46 are arranged such that the working faces 92 are aligned to be centered on a common axis of revolution AR with opposed working faces 92 that are mirror images of each other; and furthermore such that hammering motion is along the common axis of revolution AR. The working face 92 has a diameter DWF that is selected to determine a suitable foil length Lf and foil width Wf (see Figures 6A-6B). For example, the working face diameter DWF is 0.125", and can be used to hammer a molybdenum wire 42 having a 0.007" wire diameter Dw into a foil having a foil length Lf of approximately one eighth of an inch and a foil width Wf of slightly less (e.g., approximately 0.1"). The wire 42 is advanced between the working faces 92 of the hammers 46 by an amount selected to produce a uniform desired foil spacing FS (see Figure 7A) and stops with the wire 42 positioned along a diameter of the working face 92 (i.e., crossing the central, highest point of the working face 92, orthogonally crossing the axis of rotation AR). The wire 42 is hammered between the working faces 92 with a number N of blows in as rapid succession as possible. (It is believed that this will advantageously maximize the amount of heat in the wire 42 that is produced by the hammering.) The number N of blows is experimentally determined for a given wire material and diameter; e.g., for the 0.007" diameter molybdenum wire the number N has been determined to be 10. An important feature of the process is that for a given magnitude of energy E provided in the first blow, each subsequent blow has an energy that is at least linearly increased by the energy magnitude E over its preceding blow. For example: the first blow has an energy magnitude of E; the second blow has an energy magnitude of 2xE (2 times E); the third blow has an energy magnitude of 3xE; and so on to the final Nth blow having an energy magnitude of NxE. The increasing energy is necessary in order to produce a sharp-edged foil contour (e.g., foil edge 77); otherwise the foil will tend to flatten in the middle or even doughnut without appreciably more stretching and thinning of the foil edges 77. The energy magnitude E along with the number of blows N are experimentally determined for a given wire material and diameter so as to produce a desired foil thickness Tf. For example, the foil thickness Tf is 0.001". It has been noted that the foil edges 77 are thinned and sharpened by this wire flattening process. The resulting foil edge 77 is easily etched to yield an even sharper razor edge that is ideal for optimum sealing of the foil in vitreous material (e.g., quartz).

Top and cross-sectional views of a foil 75 resulting from the hammering stage are shown in Figures 5A and 5B, respectively. The resulting foil 75 tends to be slightly cupped (although

the illustration exaggerates this effect). Figure 4B shows idealized cross-sectional views (shading omitted for clarity) of the middle of the foil 75 after progressive hammer blows. The cross-section is taken as shown in Figure 4A, at the point where the wire 42 intersects the axis of revolution AR; for example, along the line 5B-5B of Figure 5A, however for illustrative purposes it is idealized by showing the profile as straight rather than cupped as in Figure 5B. The idealized profiles in Figure 4B progress from an un-hammered wire 42a having a wire diameter (and foil thickness)  $D_w$ , down to an N-blow foil 42f having the desired foil thickness  $T_f$  (as measured at it's center). For example, a 2-blow foil 42b shows the foil cross-sectional profile after 2 hammer blows on the wire 42; a 4-blow foil 42c shows the foil cross-sectional profile after 4 hammer blows on the wire 42; a 6-blow foil 42d shows the foil cross-sectional profile after 6 hammer blows on the wire 42; a 8-blow foil 42e shows the foil cross-sectional profile after 8 hammer blows on the wire 42; a 10-blow foil 42f shows the foil cross-sectional profile after 10 hammer blows on the wire 42 (where  $N=10$ ).

The idealized profiles in Figure 4B are merely illustrative of one possible scenario.

Various cross-sectional shapes have been observed at various points in the hammering process including the following: The progression in cross-sectional shapes goes from round to wiener shape after the first blow, with the waist portion taking the shape of the hammer faces 92. As the blows increase in energy, the working faces 92 themselves progressively compress. The overall foil 75 gets thinner, but the center again becomes thicker relative to the edges, presumably due to a hydrostatic "capturing" of the molybdenum such that the edges almost cease to flow. Cross-sectional shapes then progress from elliptical to lenticular in nature. Toward the end of the process it may be that the compressive forces over the whole active area are very high, but are higher in the center than at the edges of the working faces 92, thus producing the cupped effect when expansion occurs after relief of the pressure of the last blow. As the foil 75 gets thinner and thinner it resists plastic flow more and more. Lengthwise elongation decreases, and with further blows beyond N, the extruded foil along the length continues to thin until it is too fragile to be useful.

Because of longitudinal pressure on the tapered surface of the wire 42 where it transitions from the foil to the wire, the wire 42 tends to elongate even more than the foil width. During the hammering process the lead processing line 40 should provide a suitable bias force on the wire 42 to prevent longitudinal rippling or folding of the foil; for example the advancing gripper 56



can advance further during hammering, or can incorporate a spring tensioner while the spool brake 45 resists. Preferably provisions are made to keep the hammers 46 centered in the foil 75 to avoid a longitudinally asymmetric foil 75; for example the hammers 46 are advanced a predetermined amount after each hammer blow, or the spool brake 45 pulls the wire 42 backward a predetermined amount after each hammer blow while the advancing gripper 56 pulls the wire 42 forward an equal predetermined amount.

An exemplary reduction to practice (not specifically illustrated) of the inventive hammering process comprised a hammering drive 47 with the bottom hammer 46b mounted on a massive, rigid base, and the top hammer 46a slidably mounted in a vertical guide channel. In lab tests, the top hammer 46a was raised a height H and dropped for the first blow, raised a height 2xH and dropped for the second blow, and so on until it was raised a height 10xH for the final 10<sup>th</sup> blow. Thus the energy provided by the falling weight increased linearly for each blow in proportion to the height of the fall. In another reduction to practice test, the top hammer 46a was in turn hammered by a hammering drive 47 comprising a swinging hammer attached to a leaf spring that was raised against spring force by a constant-speed rotating cam wheel incorporating 12 cam steps. Each of the first ten cam steps raised and then released the spring, but the eleventh and twelfth cam steps held the spring and the top hammer 46a up slightly to allow advancing the wire 42. Each of the first ten cam steps raised the spring more than the preceding cam step in a linear progression, thereby yielding a geometric progression in hammering energy (proportional to the square of the spring raising distance, and therefore more than linear). It is anticipated that the inventive hammering process can be implemented with many different forms of hammering drive 47 including, for example, hammering drives 47 that use electromagnetic/solenoidal force rather than the above-described exemplary mechanical methods.

Referring to Figures 3, and 5A-6B, a second stage of the lead manufacturing process is a foil straightening stage that preferably also includes flame etching of the foil. Foil straightening is desired because the hammering process tends to produce a slightly cupped contour for the foil 75 as shown in Figures 5A and 5B (cupping illustratively exaggerated). For example, a first face 84a is concave while the other, second face 84b, is convex. The cupped foil 75 is bistable (concave-convex), can angle the wire 42 on either side out of collinearity, and may not present the best shape for sealing. However, when straightened according to the invention, the cupped foil 75 becomes a straight foil 76 that has advantageous stiffening edges 77'. In the preferred

embodiment, heat for the second stage is provided by a burner 48 having a flame 49 that is positioned for heating the cupped foil 75 after the cupped foil 75 is advanced out of the hammers 46. The flame 49 is long enough to accommodate movement of the cupped foil 75 as the wire 42 and cupped foil 75 elongate during the cycle due to hammering and straightening. The flame 49 is optionally extended, and further optionally segmented, in order to heat a plurality of foils 75, 76 at a plurality of foil step locations in order to continue heating the foils 75, 76 for a plurality of cycle times. Foil straightening is accomplished by applying a tensile force on the wire 42 and thus on the cupped foil 75 (e.g., by means of the advancing gripper 56), preferably while heating the cupped foil 75. A side benefit of the inventive foil straightening process is that the wire 42 can also be straightened, if necessary, by the same process. The foil 76 resulting from the foil straightening process is shown in top and cross-sectional views in Figures 6A and 6B, respectively. The elliptical dish shape of the cupped foil 75 has been stretched flat on the two longitudinal ends, and in the foil middle. The sharp edges 77 have been stretch straightened out-of-round and tend to curl around a longitudinal line to produce substantially longitudinally linear, curled edges 77' that provide collinearity for inner lead wire 82 and outer lead wire 83, and bending stiffness for the foil 76, and therefore for the foliated lead 74. Although the edges 77 are stretched the most, the overall foil length also increases slightly from a cupped foil length  $L_{cf}$  to a foil length  $L_f$ , both lengths being measured between the two locations where the foil 75, 76 starts to transition from the foil thickness  $T_f$  to the wire diameter  $D_w$ . Thus the inventive straightening process provides a simplified, improved method for achieving many of the same benefits of prior art foil stiffening methods such as that disclosed in the Karikas '356 patent. The curled edges 77' both generally curl toward the same foil face (e.g., first face 84a), therefore they do not exactly center the foliated lead 74 in a light source body (e.g., body 22) before sealing in the same way as the bi-folded foils of Karikas. However, the inventor has determined that centering occurs anyway with the present foliated leads 74 when the body 22 is sealed about the foil 76, and furthermore the foliated leads 74 also provide desired alignment of the foliated lead 74 with the necked-in portion 14 and therefore with the body 22.

A further advantage of the inventive foliated leads 74 made according to the inventive hammering process is the shape of leading/trailing ends 88 of the foil 76. The resulting tapered or at least rounded-off shape of the leading/trailing ends 88 is a feature of the inventively hammered foil 76 that eases threading of the foliated lead 74 into a close-fitting tube (e.g., the

necked-in portions 14 of the light source body 22).

In the art of making light source sealing foil, it is known that the best edge for sealing is obtained by etching a flattened metal strip, regardless of the method used for that flattening. Two methods for foil etching are chemical or electrochemical etching, and flame etching (using an oxidizing flame to burn away metal). A disadvantage of flame etching is that it leaves an oxide coating that may interfere with sealing. Therefore, a third stage of the lead manufacturing process is a foil etching stage preferably using an electrochemical etching process that will also clean any oxide coating off of the foliated wire 43, and may even etch more efficiently when the foliated wire 43 has been oxidized previously. Therefore, an optional alternate embodiment of the lead manufacturing process uses an oxidizing flame for the flame 49 to combine flame etching with foil straightening. Further alternate embodiments of the lead manufacturing process replace electrochemical etching with an oxidizing flame 49 for flame etching followed by cleaning by, for example, heating in a reducing atmosphere such as forming gas.

The preferred embodiment of the lead processing line 40 incorporates an electrochemical etching process for a third, foil etching stage of the lead manufacturing process. Referring to Figures 3, 7A and 7B the third stage comprises a first etching bath 50a followed by a second etching bath 50b (collectively referred to as etching baths 50), followed by a rinsing bath 52, and finally followed by a dryer 54. The first and second etching baths 50a, 50b are respectively filled to a first and second fluid level 86a, 86b with an electroetching fluid 53a, 53b collectively referred to as electroetching fluid 53 (e.g., an alkali such as sodium hydroxide). In order to preclude possible damage to the foils 76, the foliated wire 43 follows a conveyance path that passes straight through the etching baths 50 and the rinsing bath 52 instead of being redirected down into and up out of each bath by a typical series of rollers or pulleys. The straight-through conveyance path is enabled by passing the foliated wire 43 through relatively liquid-tight grommet seals 72 that are mounted within holes 51 below the fluid level 86a, 86b in both longitudinal ends of each bath 50a, 50b, 52. The grommet seal 72 is made of a resilient material (e.g., rubber, plastic, etc.) having a slit 73 that flexes sufficiently to allow passage of the foliated wire 43 through the grommet seal 72, but still holds the slit 73 closed enough to prevent significant fluid loss leaking through from the bath 50a, 50b, 52. Leaked fluid can be replenished by capturing it and pumping it back into the bath 50a, 50b, 52, or simply by replacement with fresh fluid, thereby maintaining constant caustic concentration. An exemplary grommet seal 72

was produced by using a short length of soft rubber, thick walled tubing with a pinch-clamp. Compression by the pinch-clamp produced the slit 73 and the electroetching fluid 53 provided an excellent lubricant. It is within the scope of the present invention to abut the ends of successive baths 50a, 50b, 52 and to use a single grommet seal 72 between each pair of abutted baths 50a, 50b, 52. Furthermore, said abutment should be herein construed to include combination of the abutted ends into a single dividing wall. Alternatively, the single grommet seal 72 between successive baths 50a, 50b, 52 could be a short length of small diameter tubing, possibly pinched to form a slit 73, the tubing extending between the holes 51 in the ends of the successive baths 50a, 50b, 52.

Chemical etching is enhanced by electrolysis using an inventive two-bath AC (alternating current) electrolysis method that doesn't require a mechanical connection of electrical power to the foliated wire 43, again in order to avoid damage to the foliated wire 43, and also to increase reliability and efficiency. One pole of an AC electrolysis power supply 66 is connected by a first supply wire 68a to a first electrode 70a in the first etching bath 50a, and the opposite pole of the electrolysis power supply 66 is connected by a second supply wire 68b to a second electrode 70b in the second etching bath 50b. The circuit is completed, for example, by electrical current being conducted by ions in the electroetching fluid 53a in the first etching bath 50a from the first electrode 70a to the foliated wire 43 in the first etching bath 50a, the current then being conducted by the foliated wire 43 from the first etching bath 50a to the second etching bath 50b, the current then being conducted by ions in the electroetching fluid 53b in the second etching bath 50b from the foliated wire 43 in the second etching bath 50b to the second electrode 70b. In the succeeding half cycle of AC, the current flow is reversed. Electrolytic etching of the foliated wire 43 alternates between the first and second etching baths 50a, 50b depending upon the direction of current in the etching bath 50. A first bath length BL1 and a second bath length BL2 are selected to provide a total etching bath length (BL1 + BL2) sufficient to allow enough machine cycle times for each foil 76 to be etched as desired while it steps through the etching baths 50. The first and second etching bath lengths BL1, BL2, respectively, are preferably approximately equal in order to balance the current density in the two baths 50a, 50b. An advantage of the inventive two-bath etching method is that the current carried between baths 50a, 50b by the foliated wire 43 can be relatively high because of the cooling provided by the electroetching fluid 53, especially when the baths 50 are connected by a single grommet seal 72,

thereby preventing exposure of the foliated wire 43 to air between the baths 50.

Referring to Figure 3, after passing through the etching baths 50, the foliated wire 43 (now etched) is passed straight through the rinsing bath 52. Other than inventively passing the foliated wire 43 through the rinsing bath 52 by means of grommet seals 72 as described for the etching baths 50, the rinsing bath uses conventional means to rinse electroetching residue from the foliated wire 43 (e.g., using de-ionized water). A length of the rinsing bath 52 is selected to allow enough machine cycle times for each foil 76 to be rinsed as desired while it steps through the rinsing bath 52. After passing through the rinsing bath 52 the foliated wire 43 is passed through a conventional dryer 54 (e.g., hot air) that is preferably non-oxidizing.

Figures 3 and 8A-8E illustrate a final, fourth stage of the lead manufacturing process that comprises a cutting stage. After the foliated wire 43 passes through the foil etching stage, the foliated wire 43 is advanced by the advancing gripper 56 and pushed out through the stationary gripper 58 and a cutter 60. At a point during the machine cycle when the advancing gripper 56 is not moving, and the length of foliated wire 43 protruding beyond the blade edges 63 is sufficient to yield a predetermined foliated lead length  $L_{fl}$  after cutting, the stationary gripper 58 optionally closes to hold the foliated wire 43 while the cutter 60 closes to cut a foliated lead 74 off the end of the foliated wire 43. The newly manufactured foliated lead 74 is made available for further light source manufacturing processes, optionally by allowing it to fall into a collection tray 64; but preferably by using a transfer 62 (e.g., vacuum head on swing arm) to hold the foliated lead 74 as it is cut off and to then move it into the collection tray 64 or on to a next portion of a light source assembly line.

An inventive cutting process produces straight cut ends 78a or angled cut ends 78b (collectively referred to as cut ends 78) on the foliated lead 74 that respectively have intentionally-formed double-sided spurs 80a, or a one-sided spur 80b (80a and 80b being collectively referred to as spurs 80). The spurs 80 protrude laterally beyond the diameter of the wire 42 that becomes a lead wire 82, 83 (e.g., the inner lead wire 82) of the foliated lead 74, and the spurs 80 are then utilized to improve subsequent assembly and handling operations as will be described hereinbelow. The cutter 60 has a top blade 59a and a bottom blade 59b (collectively referred to as cutter blades 59) that are preferably identically shaped with a blade edge 63 defined at the vertex of a left blade side 61a and a right blade side 61b (collectively referred to as blade sides 61). The cutter 60 has a central plane CP, and the top blade 59a is positioned above the

bottom blade 59b such that both blade edges 63 lie within the central plane CP. Furthermore, the cutter 60 has a configuration wherein cutting motion of the cutter 60 is such that the cutting blade edges 63 move substantially within the central plane CP, thereby bringing the blade edges 63 together to cut the foliated wire 43. In general, the best spurs 80 are produced by cutting with  
5 dull-edged (i.e., blunt) cutting blade edges 63 such that the cutting process is one of essentially "mashing apart" the foliated wire 43 as with dull nippers. Preferably the blade sides 61 are substantially straight and form a relatively broadly sloped blade angle  $\alpha$  at the vertex (blade edge 63), the blade angle  $\alpha$  being in the range of about 60°-120°, most preferably about 90°.

Preferably the blade sides 61a, 61b are reflected across the central plane CP, i.e., each is at an  
10 angle of  $\alpha/2$  from the central plane CP. The foliated wire 43 is positioned in the cutter 60 such that a wire 42 portion at a predetermined distance from the nearest foil 76 (e.g., an inner lead length  $L_{il}$ ) is between the blade edges 63. In a vertical direction, the wire 42 is perpendicular to the central plane CP. In a horizontal direction, the wire 42 is at a cut angle  $\theta$ . Figures 8B and 8C show the straight cut end 78a that results from cutting at a cut angle  $\theta$  equal to about 90°.

15 Because of the shape of the cutter blades 59 with relatively broadly sloped blade sides 61, the round wire 42 is pinched in, which causes displaced wire material to extrude outwards by a protrusion distance of PD on each side (measured radially), thereby creating the double-sided spurs 80a. Figures 8D and 8C show the angled cut end 78b that results from cutting at a cut angle  $\theta$  that is acute, preferably about 45°-75°, most preferably about 60°. Because of the shape  
20 of the cutter blades 59 with relatively broadly sloped blade sides 61, the round wire 42 is pinched in, which causes displaced wire material to extrude outwards by a protrusion distance of PD (measured radially), thereby creating the one-sided spur 80b. In addition to the one-sided spur 80b that protrudes laterally on the side of the acute cut angle  $\theta$ , the other side of the angled cut end 78b is rounded toward the center of the wire 42, thereby creating a point 79 at the outermost  
25 end of the lead wire 82, 83. The angled cut end 78 is most preferred for the present invention because it not only has the spur 80 but also the point 79, both of which provide advantages in subsequent assembly and handling operations according to the invention as will be described hereinbelow. Trials of the inventive cutting process using 0.007" diameter molybdenum wire 42 resulted in spurs 80 having a protrusion distance PD of approximately 0.001".

30 Figure 8E shows the foliated lead 74 that results from a preferred embodiment of the inventive lead manufacturing process implemented on the lead processing line 40. The foliated

lead 74 has an overall foliated lead length  $L_{fl}$ , is formed from one continuous piece of material (originally the wire 42), and comprises a single foil 76 (for sealing in a light source body, e.g., body 22) bookended by an outer lead wire 83 and an inner lead wire 82. The foil 76 has curled edges 77', a foil length  $L_f$ , and a foil width  $W_f$ . The outer lead wire 83 has an outer lead length  
5 Lol and a diameter equal to the wire diameter  $D_w$  of the wire 42. The inner lead wire 82 has an inner lead length  $L_{il}$  and a diameter equal to the wire diameter  $D_w$  of the wire 42. Both lead wires 82, 83 outwardly end in cut ends 78, preferably angled cut ends 78b that have a point 79 and a spur 80.

The lead processing line 40 has been described as a single, complete multistage line, but  
10 it should be recognized that the scope of the invention is intended to include the use of individual stages of the line, possibly separated from other stages by means of collecting the foliated wire 43, for example, on a reel of sufficient diameter to preclude introducing permanent bending or other damage to the foliated wire 43; and then unreeling the foliated wire 43 from the reel to continue the lead processing elsewhere.

#### 15 **Filament Assembly**

Figures 9A-9C show an improved process for manufacturing filament assemblies (e.g., filament assembly 104 in Figure 9C) for light sources (e.g., filament tubes, arc tubes) wherein two foliated leads 74 (first foliated lead 74a and second foliated lead 74b) are assembled together with an incandescent lamp filament (e.g., filament 102) therebetween and prepared for assembly  
20 with a light source body (e.g., body 22). This process is preferably automated to minimize manufacturing cost, and to provide dimensional consistency from part to part. Furthermore, one or more filament assembly processes can be incorporated as a portion of an assembly line, preferably automated, that makes light sources and lamps according to the invention.

Figure 9A shows a primary coil 100 comprising a filament wire 108 that is wound on a  
25 primary mandrel 106, preferably with periodically varied coiling pitches  $P_1$ ,  $P_2$ ,  $P_3$ , thereby creating a continuous length of primary coil 100 having a repeating sequence of: a first spud portion 110a, preferably followed by a first stretched-out portion 112a, followed by an incandescent portion 114; and then preferably followed by a second stretched-out portion 112b. The sequence repeats beginning with a second spud portion 110b. It should be noted that the  
30 spud portions 110a, 110b (collectively referred to as 110) are each cut in half when a filament 102 is created from the primary coil 100. Referring also to Figure 9B, the preferred embodiment

of the present invention includes a 50 W (watt), 60 V (volt) filament 102 that utilizes a coiled coil portion 115 for the incandescent part of the filament 102. It should be recognized that light sources according to the present invention may have other wattage/voltage combinations, and can be achieved, for example, with single coil filaments, and with or without a stretched-out portion

5. 112a, 112b (collectively referred to as 112).

For the preferred embodiment, the primary mandrel 106 is molybdenum wire having a mandrel diameter  $D_m$  (e.g., 0.007"), and the filament wire 108 is tungsten filament wire having a filament wire diameter  $D_{fw}$  (e.g., 0.0025"). The incandescent portion 114 is the longest portion of the primary coil 100, being long enough to accommodate the length of filament wire required for a particular voltage/wattage/life design. The coiled coil portion 115 has a coiled coil pitch  $P_4$ , and a coiled coil outside diameter  $D_{cc}$  (e.g., 0.042") that are determined according to conventional design principles. An incandescent primary coil pitch  $P_3$  is also determined according to conventional design principles. A spud portion pitch  $P_1$  is preferably equal to the incandescent primary coil pitch  $P_3$ . A stretched-out portion pitch  $P_2$  is stretched as much as possible to result in, for example, up to three lazy turns in a stretched-out portion length  $L_{st}$ . The spud portion 110 has a spud portion length  $L_{sp}$  of approximately twice the length desired for a spudding operation to be described hereinbelow. If desired, the continuous length of primary coil 100 may be annealed on the primary mandrel 106 before secondary coiling.

The filament 102 is formed by: (a) extending a first leg 116a comprising a first spud coil 111a (being half of the first spud portion 110a) plus a first stretched-out leg 113a; (b) secondary coiling, i.e., winding one incandescent portion 114 of the primary coil 100 around a removable secondary mandrel (conventional, not shown) to form the coiled coil 115; (c) extending a second leg 116b comprising a second stretched-out leg 113a plus a second spud coil 111a; (d) removing the secondary mandrel; (e) cutting the primary coil 100 in the approximate middle of the second spud portion 110b; and (f) dissolving the primary mandrel 106. Sintering of the coiled coil 115 may be done according to conventional practice, e.g., between steps (e) and (f), or possibly after the following optional step (g). An optional step (g) after dissolving the primary mandrel 106 is to further stretch and straighten the first and second stretched-out portions 112a, 112b in order to form first and second legs 116a, 116b that are almost-straight single strands of filament wire 108 having a stretched-out leg length  $L_{st}'$  that may be significantly longer than the stretched-out portion length  $L_{st}$  of the primary coil 100. This optional step (g) can be used to create stretched-



out legs 113a, 113b even when the stretched-out portions 112 of the primary coil 100 are not stretched (i.e., the stretched-out portion pitch P2 is equal to the incandescent primary coil pitch P3). In step (e) each filament 102 is cut off an end of the continuous length of primary coil 100 by means of cutting the primary coil 100 in the approximate longitudinal center of a spud portion 110, thereby creating filament spud coils 111a, 111b (collectively referred to as 111) that are approximately half the length of the spud portions (i.e., spud coil length  $L_{sp}$  is approximately half of the spud portion length  $L_{sp}$ ).

Referring to Figures 9B and 9C, the filament assembly 104 comprises a filament 102 that is assembled together with a first foliated lead 74a and a second foliated lead 74b. The first foliated lead 74a has a first inner lead 82a, a first foil 76a, and a first outer lead wire 83a. The second foliated lead 74b has a second inner lead 82b, a second foil 76b, and a second outer lead wire 83b. As described hereinabove, each of the foliated leads 74 has two cut ends 78, and each cut end 78 has at least one spur 80, and preferably a point 79 (when the cut end 78 is the preferred angled cut end 78b). The foliated leads 74 are made using wire that becomes the inner lead wires 82a, 82b and has a wire diameter  $D_w$ . The inside diameter of the spud coils 111 is approximately the same dimension as the primary mandrel diameter  $D_m$  upon which they were wound. For the preferred embodiment illustrated in Figure 9B, the first inner lead wire 82a of the first foliated lead 74a is shown as it is being assembled with the filament 102, and the second inner lead wire 82b of the second foliated lead 74b is shown after being assembled with the filament 102. The illustrated assembly is accomplished by a spudding process wherein the cut end 78 of an inner lead wire 82 becomes a "spud" that is inserted into a tight fitting spud coil at the end of a leg 116 of the filament 102. Although spudding is known, the present invention provides an improved spudding process due to inventive features of the inner lead wire 82. In particular, the inner lead wire outside diameter  $D_w$  is approximately the same as, or slightly more than, the spud coil inside diameter  $D_m$ ; and the one or more spurs 79 on the cut end 78 provide a lateral protrusion that serves as a screw thread such that the cut end 78 can be "screwed" into the spud coil 111 and the spur(s) 79 will thereafter hook onto a turn of the spud coil 111. Because of this hooking, it is not necessary to make the inner lead wire outside diameter  $D_w$  significantly larger than the spud coil inside diameter  $D_m$ ; and it is also not necessary to weld the spud coil 111 to the inner lead wire 82. A further advantage accrues when the cut end 78 is the preferred angled cut end 78b with a point 79, in which case the point 79 (which tends to be somewhat

indented from the outside diameter of the inner lead wire 82) is used to funnel the cut end 78 into the spud coil 111, and will also help to wedge the spud coil open if it is tight.

### **Light Source Finishing**

Figures 10A-12C and Figures 15A-15B illustrate preferred embodiments of an improved finishing process for manufacturing light sources (e.g., filament tube 218 in Figures 10E and 13A, e.g., arc tube 318 in Figures 15B and 13B) for lamps wherein a filament assembly (e.g., 104) or a pair of arc tube electrodes (e.g., first and second electrodes 306, 308 in Figure 15A) is positioned in a light source body (e.g., body 22) that is flushed and/or exhausted, filled, sealed about foils 76, and otherwise finished. This light source finishing process is preferably automated to minimize manufacturing cost, and to provide dimensional consistency from part to part. Furthermore, one or more light source finishing processes can be incorporated as a portion of an assembly line, preferably automated, that makes light sources and lamps according to the invention.

The improved light source finishing process is inventive in that inventive equipment (e.g., a filament tube light source finishing stand 148, as in Figure 10B, or an arc tube light source finishing stand 148', as in Figure 15A) utilizes inventive features of component parts of the inventive light sources described herein. Exemplary embodiments of the inventive light source finishing process will be described hereinbelow, the process comprising at least partial evacuation, flushing, filling, and sealing of a light source (e.g., filament tube or arc tube). The described process embodiments are exemplary of a variety of finishing process methods and schedules, including both pump-flush and/or through-flush methods, that can be accommodated by the inventive light source finishing equipment. Likewise, the illustrated light source finishing stands 148, 148' are exemplary embodiments of a variety of configurations of light source finishing equipment that can incorporate elements and features of the inventive equipment and light source components.

Figure 10A shows a finishing head 150 in a cross-sectional view, and Figures 11A and 11B are a top view and a side cross-sectional view, respectively, that show details of an inner tube assembly 172 that is part of the finishing head 150. Also shown is an exemplary filament assembly 104, suitable for use with the finishing head 150, that has been positioned in the finishing head 150 according to the invention. For the sake of clarity, the filament assembly 104 is not cross-sectioned in the side views, and the vitreous material of the body 22 is left un-shaded

in the cross-sectional views. The finishing head 150 is also referred to as a top finishing head 150 due to configuration differences that distinguish it from a colletless bottom finishing head 151 (see Figure 10B) and a colleted bottom finishing head 151' (see Figure 15A).

The finishing head 150 comprises a block 160 of a suitable material (e.g., stainless steel, and/or with anticorrosive plating) that has a cylindrical central chamber 162 with a cylindrical axis CA. The chamber 162 is open on one end (e.g., the bottom) that is further drilled to accommodate the inner tube assembly 172 as described hereinbelow. At least two inlets 158 (e.g., first inlet 158a and second inlet 158b) access the chamber by means of respective first and second needle valves 155a, 155b, comprising a first needle valve stem 156a with a first needle valve orifice 157a, and a second needle valve stem 156b with a second needle valve orifice 157b. The first and second inlets 158a, 158b and their respective first and second needle valves 155a, 155b are designed according to the type and flow rate of gas(es) that they will be handling. Preferably the first and second needle valves 155a, 155b (collectively referred to as needle valves 155) are automatically manipulated and are suitable for shutting off as well as controlling flow rate.

Coaxial to the chamber 162 is an annular recess 163, also open on the same one end as the chamber 162. A cylindrical spring bellows 164 is sealingly attached to the closed end of the annular recess 163, preferably being attached near a radially outermost periphery of the annular recess 163, such that a shroud gas line 152, controlled by a valve 154, can open into the annular recess 163 but radially within the spring bellows 164. The open end of the spring bellows 164 is sealingly attached to a washer-like flat annular floating plate 166 that is in turn sealingly attached to an outer tube 168. The outer tube 168 coaxially surrounds the central chamber 162 and thus shares its cylindrical axis CA. The outward (e.g., bottom) edge 169 of the outer tube 168 is a thinned edge 169 for flexibility. The spring bellows 164 functions as a compression spring for biasing the outer tube 168 downward in a direction roughly parallel to the cylindrical axis CA. An inner tube assembly 172 is coaxially mounted in the open end of the chamber 162, with an inner tube 170 protruding beyond (below, further outward of) the outer tube 168. The outward (e.g., bottom) edge 171 of the inner tube 170 is a thinned edge 171 for flexibility. The thinned edges 169, 171 are thinner than the remainder of the respective tubes 168, 170, but not so thin as to become a sharp knife edge because that is too weak. For example, rather than feathering the edge, it can be turned down to make a uniformly thinner wall tube 168, 170 at the thinned edge

169, 171, and the outermost end can be polished blunt to ruggedize the thinned edge 169, 171 due to the blunt end at the same time that the polishing helps assure good sealing with the bugled end 16 of the body 22. It should be noted that various equivalent structures can achieve the described purposes of the spring bellows 164 and the floating plate 166, such as, for example, a  
5 springy annular disc-like diaphragm, or for example a separate spring plus an extendable bellows for sealing.

Both the inner tube 170 and the outer tube 168 are made from relatively thin walled metal tubing (e.g., stainless steel). Referring to Figure 10D, it can be seen that the use of metallic components (e.g., 168, 170, 190) for sealingly connecting the finishing head 150 to the body 22  
10 allows for sealing bodies 22 that have relatively short lengths of material between the finishing head 150 and a necked in body portion 14 that is heated by a high temperature sealing burner 220 to seal around the foil 76. Thus the inventive bugled end 16 in combination with the inventive finishing heads (e.g., 150) minimizes the amount of expensive vitreous material that is consumed in the manufacture of a finished light source.

Referring now to Figures 11A and 11B, the inner tube assembly 172 is a stacked  
15 assembly of coaxial components comprising a collet 174, which is stacked on a spacer ring 186, which is stacked on a funnel ring 188, which is stacked on the inner tube 170. The inner tube 170 is sealingly attached to the chamber 162 in a way that makes an approximately gas-tight seal between the innermost (upper) end of the inner tube 170 and the chamber 162 (e.g., by press  
20 fitting into a slightly tapered hole). Vertical positioning of the inner tube 170 is accomplished by means of a reduced diameter spacer stop 202. The collet 174 is vertically positioned by being trapped between the spacer ring 186 and a collet stop 200 at the top. The funnel ring 188 is optional and can be used to assist in loading the outer lead wire 83b of the filament assembly 104 into the collet 183. The funnel ring 188 is substantially a conical washer oriented for funneling  
25 the outer lead wire 83b into a center hole 183 of the collet 174. The spacer ring 186 is also optional, being an annular ring that cooperates with the optional funnel ring 188 in order to position the collet 174 suitably spaced above the funnel ring 188. Further funneling effect is achieved by a bottom bevel 185 that leads into the center hole 183. Even further funneling effect is achieved when, as illustrated, the cut end 78 of the outer lead wire 83b is an angled cut end  
30 78b having a radially inset point 79 and an acute cut angle  $\theta$  (see Figure 8D). Without the optional funnel ring 188 and spacer ring 186, the spacer stop 202 can be repositioned such that

the inner tube 170 stops against it, thereby trapping the collet 174 between the inner tube 170 and the collet stop 200. In any case, the collet stop 200 and the spacer stop 202 should be positioned such that the collet 174 is loosely trapped for allowing free and easy radial expansion/contraction movement of the collet 174 and its component parts.

5       The collet 174 is a spring-closed type of self-closing collet comprised of three substantially equal sectors 180a, 180b, 180c (collectively referred to as collet sectors 180) that are held together by a circumferentially extending circumferential spring 178 (e.g., a snap ring or an o-ring), which is captured in a spring groove 179. The collet 174 is substantially cylindrical and has a coaxial center hole 183. Gas passage through the collet 174 is enabled by longitudinal  
10   holes 176 through the collet sectors 180 and/or by longitudinal slots 182 between adjacent collet sectors 180. An optional top bevel 184 is cut at a collet top 204 junction with the center hole 183 to provide a funnel for easing the pulling of spurs 80 down through the center hole 183.

There are at least two important variants of the inventive collet 174, both of which are within the scope of the present invention. The primary embodiment is illustrated in Figures 11A  
15   and 11B and will be described first. A second, alternate embodiment is a dimensional variant and possible simplification of the illustrated embodiment and therefore is not separately illustrated or numbered. The primary embodiment of the collet 174 is intended to utilize the one or more spurs 80 (i.e., the one-sided spur 80b, or the double-sided spurs 80a) for vertical positioning of the filament assembly 104. In the alternate embodiment, vertical positioning must  
20   be established by other, external means (e.g., a robot arm, not illustrated, that inserts the outer lead wire 83b into the collet 174 to a predetermined vertical position).

When the collet sectors 180 are held together such that the collet 174 is fully closed, the center hole 183 has an inside diameter  $D_c$ . For the illustrated primary embodiment, the hole diameter  $D_c$  is dimensioned to be at least equal to, and preferably slightly larger than, the  
25   diameter  $D_w$  of the outer lead wire 83b, but not as large as the overall width of the wire diameter  $D_w$  plus one protrusion distance  $PD$  for the spur 80. (If double spur straight cut ends 78a are being used, then the hole diameter  $D_c$  can be almost as large as the wire diameter  $D_w$  plus two protrusion distances  $PD$ .) It can be seen that the collet 174, so dimensioned, will open radially against the circumferential spring 178 as the spurred cut end 78 is pushed up through the collet  
30   174. Once the spur 80 has passed into the chamber 162 above the collet 174, the collet 174 will close around the outer lead wire 83b to loosely hold it approximately centered along the

cylindrical axis CA. When the outer lead wire 83b is released, it will drop down until the spur 80 hangs on the collet top 204, thereby providing vertical positioning of the filament assembly 104. If a top bevel 184 has been provided, then depending on its dimensions, the top bevel 184 may be the portion of the collet top 204 upon which the spur 80 hangs. The collet 174 and the chamber 162 are suitably dimensioned such that the collet 174 has room to radially expand as needed, but not too much room so that the collet 174 remains approximately centered along the cylindrical axis CA.

For an alternate embodiment of the collet 174, the hole diameter  $D_c$  is dimensioned to be slightly smaller than the diameter  $D_w$  of the outer lead wire 83b. In this case, the collet 174, so dimensioned, will open radially against the circumferential spring 178 as the cut end 78 (with or without spurs 80) is pushed up through the collet 174. Once the cut end 78 has passed into the chamber 162 above the collet 174, the collet 174 will close around the outer lead wire 83b to grip and hold it approximately centered along the cylindrical axis CA. When the outer lead wire 83b is released, it will be held by the collet 174 to maintain a predetermined vertical positioning of the filament assembly 104.

With reference to Figures 10A, 10B, and 11C, the finishing head is further equipped with a left clamshell 190a and a right clamshell 190b (collectively referred to as clamshells 190) for positioning and holding the light source body 22 by acting on the inventive bugled end 16. The clamshells 190 are rectangular plates, each having an abutting edge 196 where the left and right clamshells 190a, 190b abut when the clamshells 190 are closed (as in Figures 10B and 11C). Figures 10A and 11C illustrate a first embodiment of the clamshells 190 wherein the clamshells 190 are hingedly connected to a frame 189 by means of hinges 191. Preferably the frame 189 is vertically (longitudinally) fixed or more preferably is spring biased against the finishing head 150, but is free to slide a predetermined amount in any direction within a horizontal (lateral) plane. Figure 10A shows the hinged first embodiment of the clamshells 190 in an open position, swung downward to create an opening large enough to accept the bugled end 16 of a body 22. Figures 12A-12C show a second embodiment of the clamshells 190 wherein the clamshells 190 are not hinged, but instead slide horizontally, preferably left and right on a frame 189 that is vertically fixed or more preferably is spring biased against the finishing head 150, but is free to slide a predetermined amount in any direction within a horizontal plane. Figure 12A shows the sliding second embodiment of the clamshells 190 in an open position, slidably pulled apart such

that the abutting edges 196 are spaced apart enough to accept the bugled end 16 of a body 22, but the left clamshell 190a remains aligned in a common plane with the right clamshell 190b. It should be understood that the scope of the invention is intended to include all equivalent means for opening and closing the clamshells 190. For example, the horizontal sliding movement could be in an arc driven by a scissor-like mechanism.

Referring now to Figure 11C, both embodiments of the clamshells 190 provide a circular opening, i.e., a center hole 194 for receiving a bugled end 16, wherein each clamshell 190a, 190b has a semicircular opening cut out of its abutting edge 196. When the clamshells 190 are closed as shown, with their abutting edges 196 abutted, the center hole 194 has a minimum diameter  $D_n$  that is slightly less than a bugled end average diameter  $D_b$  (see Figure 12A), such that closing the clamshells will trap a bugled end 16, pushing upwards on the bugled end 16 to hold it against the finishing head 150. A sloped sided, preferably spherical, cavity is formed in the closed clamshells 190 such that the spherical cavity creates an annular spherical cavity wall 192 having a maximum diameter  $D_x$  where it joins a top (inner) surface 198 of the clamshells 190, and a minimum diameter  $D_n$  where it joins a bottom (outer) surface 199 (see Figure 10A) of the clamshells 190, thereby creating the center hole 194. The remaining portions of the abutting edges 196 are preferably trimmed back a bit so that the clamshells 190 can be closed around undersized bugled ends 16. As shown in Figure 12A, the bugled end 16 of the light source body has an average diameter  $D_b$ . The clamshells 190 are dimensioned such that the maximum diameter  $D_x$  is slightly greater than the bugled end average diameter  $D_b$ , and the minimum diameter  $D_n$  is slightly less than the bugled end average diameter  $D_b$ . The curvature of the cavity wall 192 matches the locus of points traced by the outermost parts of the bugled end 16 as the bugled end 16 is tilted while pressed up against the inner tube 170, i.e., tilting a body cylindrical axis CAB relative to the inner tube cylindrical axis CA as shown in Figure 12B.

Actual clamshell dimensions are easily fine-tuned to assure proper operation of the clamshells 190 according to the invention as further described with reference to Figures 12A-12C, which show a side cross-sectional view of relevant portions of the finishing head 150 and of a light source body 22 as it is being loaded into the finishing head 150. The illustrated portions of the finishing head 150 include an outer portion of the inner tube 170 with its thinned edge 171, surrounded by the outer tube 168 with its thinned edge 169, an outer portion of the spring bellows 164 that is attached to the outer tube 168 by means of the floating plate 166, and

clamshells 190 with their frame 189. Operation of the clamshells 190 is illustrated for a sliding embodiment, but similarly applies to operation of the hinged embodiment of the clamshells 190. The inner tube 170 has a cylindrical axis CA and the outer tube 168 is approximately coaxial to the inner tube 170. Preferably the clamshells 190 open and close in a way that maintains equal spacing from the cylindrical axis CA to the spherical cavity wall 192 of each of the clamshells 190a, 190b.

In Figure 12A, a light source body 22 having a body cylindrical axis CAB is shown as it is being loaded into the finishing head 150. It can be seen that the body 22 is laterally off center, as well as being tilted such that the body cylindrical axis CAB is at a non-zero angle relative to the cylindrical axis CA of the finishing head 150. Figure 12B shows that as the body 22 was raised into the finishing head 150 (by a compliant holder, not shown), the bugled end 16 interacted with the inner tube 170 and was therefore laterally centered. Figure 12C shows the result of closing the clamshells 190 in a first configuration wherein the frame 189 is horizontally (laterally) fixed with the center hole 194 coaxially aligned with the cylindrical axis CA of the finishing head 150. Thus the body 22 was also aligned (i.e., the body 22 was made coaxial with the inner tube 170) by the clamshells 190 as they closed such that the spherical cavity wall 192 pressed upward on the lowest portion of the tilted bugled end 16. Furthermore, because of the shape and dimensions of the spherical cavity wall, preferably aided by a vertical spring bias on the clamshells 190, the closed clamshells 190 exert continuous inward (longitudinal) pressure on the bugled end 16, thereby maintaining firm contact between the inner tube thinned edge 171 and the inside of the bugled end 16. Also, the spring pressure of the spring bellows 164 maintains firm contact between the outer tube thinned edge 169 and the inside of the bugled end 16. In a second configuration, wherein the frame floats in the horizontal plane, it can be seen that closing the clamshells 190 will leave the body 22 tilted as shown in Figure 12B, but will press upward to hold the tilted bugled end 16 against the thinned edge 171 of the inner tube 170. This second configuration provides a certain amount of compliance for tolerating minor misalignment between a top finishing head 150 and a bottom finishing head 151 (see Figure 10B), without placing any bending stress on the body 22, and furthermore allows the combination of top finishing head 150 and bottom finishing head 151 to achieve alignment of a body 22 being held between them.

Figure 10A illustrates a first step of the light source finishing process wherein the



filament assembly 104 is loaded into the top finishing head 150 where it is suspended at a predetermined vertical position by the collet 174 as described hereinabove. If the light source is to be an arc tube (e.g., 318) rather than a filament tube (e.g., 218), then a first electrode/foliated lead assembly 302 (see Figure 15A) can be similarly loaded into the top finishing head 150.

5        Figure 10B illustrates a second step of the light source finishing process wherein the filament assembly 104 is threaded into a light source body 22, and the light source body 22 is loaded into the top finishing head 150 and also into a colletless bottom finishing head 151. Both the top finishing head 150 and the colletless bottom finishing head 151 are oriented approximately vertically (e.g., the cylindrical axis CA is approximately vertical), with the top finishing head 150 being above the colletless bottom finishing head 151. As described hereinabove, the light source body 22 is laterally centered and axially aligned with the finishing heads 150, 151 by means of the interaction of bugled ends 16 (top 16a, and bottom 16b) with clamshells 190 (top left 190a, top right 190b, bottom left 190c, and bottom right 190d) and with inner tubes 170 (top 170a, and bottom 170b). The top finishing head 150 and the colletless bottom finishing head 151 are substantially axially aligned with each other, and at least one of the two finishing heads 150, 151 is compliant in its vertical positioning in order to accommodate slight variations in overall body length L. For example: the top finishing head can be resting on a bracket (not shown). The body 22 can be loaded into the colletless bottom finishing head 151 first, wherein the bottom bugled end 16b is held by closed bottom clamshells 190c, 190d; then 20 the body 22 can be raised up around the filament assembly 104 to be loaded into the top finishing head 150, possibly raising the top finishing head 150 slightly as a top bugled end 16a presses upward against a top inner tube 170a of the top finishing head 150. In the case of floating clamshell frames 189, this will also finish aligning the body 22 relative to the combined top finishing head 150 and colletless bottom finishing head 151. The loading operation is completed 25 by closing the top clamshells 190a, 190b. The funnel shape of the top bugled end 16a helps to guide the hanging filament assembly 104 down into the body 22, further assisted by the tapered or at least rounded-off leading/trailing ends 88 of the foils 76. While raising the body 22, the filament assembly can be further encouraged to thread down into the body 22 by directing a stream of clean, dry, inert gas down into and/or through the body 22 (e.g., shroud gas emitted 30 between the top inner tube 170a and top outer tube 168a), optionally evacuated by an evacuation line 153 in the colletless bottom finishing head 151.

The colletless bottom finishing head 151 is mostly equivalent to the top finishing head 150. For example, the colletless bottom finishing head 151 has: a clamshell frame 189 with left and right bottom clamshells 190c, 190d, respectively, that are equivalent to the left and right top clamshells 190a, 190b, respectively; a bottom inner tube 170b that is equivalent to the top inner tube 170a; a bottom outer tube 168b connected by means of a bottom floating plate 166b to a bottom spring bellows 164b that is connected at an opposite end to a bottom annular recess 163b - all of which are equivalent to corresponding top components (i.e., a top outer tube 168a connected by means of a top floating plate 166a to a top spring bellows 164a that is connected at an opposite end to a top annular recess 163a); and a bottom shroud gas line 152b, controlled by a valve 154 that opens into the bottom annular recess 163b but radially within the bottom spring bellows 164b - all of which are equivalent to corresponding top components (i.e., a top shroud gas line 152a, controlled by a valve 154 that opens into the top annular recess 163a but radially within the top spring bellows 164a).

The colletless bottom finishing head 151 differs from the top finishing head 150 in ways that include the following. The bottom outer lead wire 83a may not require holding when a filament assembly 104 is suspended from the collet 174 in the top finishing head 150, therefore the colletless bottom finishing head 151 does not have a collet 174, spacer ring 186, or funnel ring 188. In place of the inlets 158a, 158b with needle valves 155a, 155b, the colletless bottom finishing head 151 has an evacuation line 153 controlled by a valve 154, that is connected to a colletless bottom finishing head chamber 173. A colletless bottom finishing head block 161 is suitably modified to accommodate the differences as compared to the block 160 of the top finishing head 150.

The top finishing head 150 and colletless bottom finishing head 151 with suitable gas, electric, and mechanical connections, combine to form an inventive filament tube light source finishing stand 148 for implementing the inventive light source finishing process, especially for filament tubes (e.g., 218).

Figure 15A illustrates a colleted bottom finishing head 151' that can be substituted for the colletless bottom finishing head 151 for use in situations wherein it is desirable to hold a bottom outer lead wire 83a (e.g., in arc tube manufacturing wherein a first electrode assembly 302 is held by the top finishing head 150 and a second electrode assembly 304 is held by the colleted bottom finishing head 151'). The colleted bottom finishing head 151' primarily differs from the colletless

bottom finishing head 151 by having a complete inner tube assembly 172 comprising the inner tube 170, the funnel ring 188 (optional), the spacer ring 186 (optional), and the collet 174. A colleted bottom finishing head block 161' and a colleted bottom finishing head chamber 173' are suitably modified to accommodate the differences as compared to their respective components in the colletless bottom finishing head 151.

The top finishing head 150 and colleted bottom finishing head 151' with suitable gas, electric, and mechanical connections, combine to form an inventive arc tube light source finishing stand 148' for implementing the inventive light source finishing process for any double ended light source wherein the two lead wires (e.g., first and second foliated leads 74a, 74b) are not assembled together, the primary embodiment of this being arc tubes (e.g., 318). The arc tube light source finishing stand 148' is essentially the same as the filament tube light source finishing stand 148 with the colleted bottom finishing head 151' being substituted for the colletless bottom finishing head 151. It should be apparent that the arc tube light source finishing stand 148' could also be used for finishing filament tubes (e.g., 218), as long as a way is provided for accommodating the bottom outer lead wire 83a of the filament assembly 104.

Referring to Figure 10B, the end result of the second step of the inventive light source finishing process that utilizes the inventive light source body 22, filament assembly 104, and finishing heads 150 and 151 (optionally 151') is as follows. The light source body 22 is sealingly held in a way that creates a closed system of the finishing heads 150, and 151 or 151' and the inside of the body 22 for at least partial evacuation, for flushing, for filling, and for lead wire sealing by means of a variety of methods and schedules. The smoothly curved inner surfaces of the bugled ends 16a, 16b are double sealed: a first seal to the thinned edge 171 of the inner tubes 170a, 170b; and a second seal to the thinned edge 169 of the outer tubes 168a, 168b. Between the first and second seals a shroud gas (an inert gas, e.g., argon) is supplied by the shroud gas lines 152a, 152b at a slightly greater pressure relative to ambient air pressure, thereby preventing contaminating ambient air from leaking into the body 22. The filament assembly 104 (and its filament 102) is axially centered in the body 22: approximately by the collet 174, and more precisely by the straightened foils 76 in the necked-in portions 14. The collet 174, preferably working with spur(s) 80, has vertically positioned the filament assembly 104 such that the foils 76 are in position for proper sealing in the necked-in portions 14, and the filament 102 is longitudinally (vertically) centered in the bulb 18. It may be noted that even heating of the body

22 during shrink sealing is required to maintain proper centering and alignment of the body 22 and the filament assembly 104.

Figure 10B also illustrates a third step of the inventive light source finishing process. In the third step, the light source body is prepared for filling by removing contaminated gases (e.g., moist ambient air) by means of, for example, a preferred flushing method or, alternately a pump-flush method. For example, with the needle valves 155 closed, a partial evacuation of the body 22 can be effected by opening the valve 154 of the evacuation line 153 and pumping on the evacuation line 153. Flushing is accomplished by opening the first needle valve 155a to allow a flushing gas to be passed through the first inlet 158a, into the chamber 162, through the holes 176 and/or slots 182 of the collet 174, through the body 22, and out the evacuation line 153. If a partial vacuum is drawn before flushing, then this process is a pump-flush method, whereas a continuous flushing while pumping on the evacuation line 153 is a through-flush method. As is known, heating the body 22 while flushing helps to drive out contaminants, and the flushing gas should be very dry. A variety of pump-flush and/or through-flush methods and schedules can be accommodated by the inventive light source finishing stands 148, 148'.

Figure 10B also illustrates a fourth step of the inventive light source finishing process: filling. Once the body 22 is sufficiently flushed, the first needle valve 155a is closed, optionally a partial vacuum is drawn by the still-open evacuation line 153, and then the second needle valve 155b is opened to allow a fill gas to be passed through the second inlet 158b, into the chamber 162, through the holes 176 and/or slots 182 of the collet 174, and into the body 22, thereby filling the body 22 with the fill gas. Once a desired proportion of the flushing gas has been replaced by fill gas in the body 22, the body 22 is ready for sealing as illustrated in Figures 10C-10F. An advantageous feature of the inventive finishing head 150 is the small internal volume and small diameter of the chamber 162 plus inner tube assembly 172 plus necked-in portion 14. Especially when combined with a small volume bulb 18, the small internal volume becomes a pipeline that allows "slugs" of nearly unmixed gases to pass sequentially through, especially since the pipeline is also a small enough diameter to promote viscous flow rather than turbulent flow. Given suitable timing of the needle valves 155, it should be possible to position a slug of fill gas in the bulb 18 at the time that a first seal is effected in a bottom necked-in portion 14b (see Figure 10C), thereby minimizing the amount of expensive fill gas (e.g., Xenon) needed to fill the bulb 18. The exact amount of Xenon gas needed could be measured out in an external calibrated

volume (not shown) that is opened into the chamber 162.

Figure 10C illustrates a fifth step of the inventive light source finishing process: making a first seal 210a. The preferred sealing method, illustrated herein, is known as "shrink sealing", although the inventive light source finishing stand 148, 148' will accommodate other methods (e.g., pinch sealing). At a time when it is determined that the body 22 has been sufficiently flushed and is being filled with the fill gas, a sealing burner 220 is applied to a bottom necked-in portion 14b of the body 22. For shrink sealing, the second needle valve 155b and/or the evacuation line valve 154 are adjusted to create a pressure within the body 22 that is near or slightly below ambient pressure, thereby assisting the shrink sealing. In Figure 10C, a top necked-in portion 14a illustrates the seal area before sealing, and the bottom necked-in portion 14b is shown at the completion of shrinking to form the first seal 210a. The size, shape, intensity, heating time, etc. for the sealing burner 220 and its flames are adjusted according to known methods for shrink sealing. Likewise, the sealing burner 220 may be oscillated for suitably applying heat around the perimeter of the bottom necked-in portion 14b. Uniform, even heating is needed in order to maintain axial alignment of the seal 210a and therefore of the filament assembly 104 within. Preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around the foil 76 of a bottom foliated lead 74b to form a hermetic seal between the body 22 and the foil 76. Further preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around a bottom inner lead 82b and at least part of a bottom spud coil 111b to form an inner lead seal 212 for assisting to hold together the bottom spud coil 111b and the bottom inner lead 82b, and also for preventing stress at the transition from the bottom inner lead wire 82b to the foil 76. Further preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around a portion of the stretched-out leg 113 of the filament 104, for quenching arcs that may occur at end of life of the filament tube. Further preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around a bottom outer lead wire 83b to form an outer lead seal 214 for preventing stress at the transition from the bottom outer lead wire 83b to the foil 76, and also for defining a preferred circular cross-section for the innermost portion of a bell mouth 216 that results from shrinking the innermost end of the bottom bugled end 16b. As will be seen in the description of light source mounting hereinbelow with reference to Figure 14, the bell mouth 216 does not have to be round, and furthermore can be quite shallow in depth, as long as there is room for an elbow 422

of an electrical support wire 416.

Figure 10D illustrates a sixth and final step of the inventive light source finishing process: making a second seal 210b (see Figures 10E-10F for views of the completed seal). After completion of the first seal 210a, a cooling nozzle 222 begins spraying a coolant 224 (e.g., liquid nitrogen) onto at least a lower portion of the bulb 18 of the body 22 in order to "freeze" a predetermined amount of the fill gas into the bulb 18. For example, the chamber 162 can be sized such that the predetermined amount equals the slug of gas contained in the closed volume comprising the chamber 162 (with needle valves 155 closed), the inner tube 170 and the sealed-one-end body 22. By closing the second needle valve 155b, freezing the fill gas will cause a below-ambient pressure within the body 22, thereby assisting in the shrink seal process. The sealing burner 220 is applied to the top necked-in portion 14a of the body 22. In Figure 10D, the top necked-in portion 14a illustrates the seal area before shrink sealing to form the second seal 210b (shown in Figures 10E-10F). The second seal 210b is formed by a shrink sealing process as described hereinabove for the first seal 210a. After forming the second seal 210b, the coolant 224 and the various gas and vacuum lines can be turned off (valves closed); the sealing burner 220 can be extinguished and/or removed; and the clamshells 190 can be opened and the completed light source (in this case a filament tube 218) can be removed from the light source finishing stand 148. Optionally a pilot flow of gas can be maintained in the chambers 162, 173 and in the outer tubes 168 as a means for releasing the seal to the bugled ends 16 and also as a means for preventing backflow contamination of the finishing heads 150, 151.

Figures 10E and 10F show two views (rotated 90° one from the other) of the filament tube 218 finished according to the invention. The first seal 210a and the essentially identical second seal 210b (collectively referred to as seals 210) are shrunk around the foils 76 of the foliated leads 74 to form hermetic seals between the body 22 and the foils 76. Preferably, the seals 210 are also shrunk around the inner leads 82 and at least part of the spud coils 111 to form inner lead seals 212 for assisting to hold each spud coil 111 together with a corresponding inner lead 82, and also for preventing stress at the transition from inner lead wire 82 to foil 76. Further preferably, sufficient heat is applied such that the inner lead seals 212 are formed around a portion of the stretched-out legs 113 of the filament 104, for quenching arcs that may occur at end of life of the filament tube 218 (i.e., quenching an arc before it can reach the more massive inner lead wire 82). Further preferably, the seals 210 are also shrunk around the outer lead wires

83 to form outer lead seals 214 for preventing stress at the transition from outer lead wire 83 to foil 76, and also for forming bell mouths 216 having a preferred circular cross-section for the innermost portion of each bell mouth 216 that results from shrinking the innermost end of each bugled end 16. As will be seen in the description of light source mounting hereinbelow with  
5 reference to Figure 14, the bell mouth 216 does not have to be round, and furthermore can be quite shallow in depth, as long as there is room for an elbow 422 of an electrical support wire 416.

The inventive filament tube light source finishing stand 148, and arc tube light source finishing stand 148' have been described hereinabove, along with process steps for finishing a  
10 filament tube 218. With reference to Figures 10A-10D and Figures 15A-15B, the process steps for finishing an arc tube 318 will now be described. In general, only a few changes are needed to adapt the inventive finishing stand and finishing process steps for finishing arc tubes instead of filament tubes.

Figures 10A and 15A illustrates a first step of the arc tube light source finishing process  
15 wherein a first electrode/foliated lead assembly 302 (instead of the filament assembly 104) is loaded into the top finishing head 150 where it is suspended at a predetermined vertical position by the collet 174 as described hereinabove. Similarly, a second electrode/foliated lead assembly 304 is loaded into the colleted bottom finishing head 151'. Vertical positioning of the second electrode/foliated lead assembly 304 can be accomplished in at least two ways. If the collet 174  
20 in the colleted bottom finishing head 151' is dimensioned to grip the bottom outer lead wire 83a, then vertical positioning is accomplished by the mechanism that places the second electrode/foliated lead assembly 304 into the collet 174. If it is desired to use a spur 80 hanging from the collet 174, then the arc tube light source finishing stand 148' can be inverted when vertical positioning of the second electrode/foliated lead assembly 304 is needed (e.g., during  
25 sealing about the foil 76 of the second electrode/foliated lead assembly 304).

Figure 15A illustrates a second step of the light source finishing process wherein the first and second electrode/foliated lead assemblies 302, 304 are threaded into a light source body 22, and the light source body 22 is loaded into the top finishing head 150 and also into the colleted bottom finishing head 151'. As described hereinabove, the light source body 22 is laterally  
30 centered and axially aligned with the finishing heads 150, 151' by means of the interaction of bugled ends 16 with clamshells 190 and with inner tubes 170. The top finishing head 150 and

the colleted bottom finishing head 151' are axially aligned with each other, and at least one of the two finishing heads 150, 151' is compliant in its vertical positioning in order to accommodate slight variations in overall body length L. The funnel shape of the bugled ends 16 helps to guide the first and second electrode/foiliated lead assemblies 302, 304 into the body 22, further assisted by the tapered or at least rounded-off leading/trailing ends 88 of the foils 76. The first and second electrode/foiliated lead assemblies 302, 304 can be further encouraged to thread into the body 22 by directing a stream of clean, dry, inert gas into and/or through the body 22 (e.g., shroud gas emitted between the inner tube 170 and outer tube 168). Also, threading of the second electrode/foiliated lead assembly 304 can be assisted by inverting the arc tube light source finishing stand 148' while the body 22 is applied over the second electrode/foiliated lead assembly 304.

Referring to Figure 15A, the end result of the second step of the inventive light source finishing process that utilizes the inventive light source body 22, first and second electrode/foiliated lead assemblies 302, 304, and finishing heads 150 and 151' is as follows. The light source body 22 is sealingly held in a way that creates a closed system of the finishing heads 150, 151' and the inside of the body 22 for at least partial evacuation, for flushing, for filling, and for lead wire sealing by means of a variety of methods and schedules. The smoothly curved inner surfaces of the bugled ends 16 are double sealed: a first seal to the thinned edge 171 of the inner tubes 170; and a second seal to the thinned edge 169 of the outer tubes 168. Between the first and second seals a shroud gas (an inert gas, e.g., argon) is supplied by the shroud gas lines 152 at a slightly greater pressure relative to ambient air pressure, thereby preventing contaminating ambient air from leaking into the body 22. The first and second electrode/foiliated lead assemblies 302, 304 (and their corresponding first and second electrodes 306, 308) are axially centered in the body 22: approximately by the collets 174, and more precisely by the straightened foils 76 in the necked-in portions 14. The collet 174, preferably working with spur(s) 80, has vertically positioned the filament assembly 104 such that the foils 76 are in position for proper sealing in the necked-in portions 14, and the first and second electrodes 306, 308 are longitudinally (vertically) positioned at predetermined locations relative to the bulb 18 (determined by shank lengths between electrodes and foils).

Figure 15A also illustrates a third step of the inventive arc tube light source finishing process. In the third step, the light source body is prepared for filling by removing contaminated



gases (e.g., moist ambient air) by means of, for example, a preferred flushing method or, alternately a pump-flush method, as described hereinabove.

Figure 15A also illustrates a fourth step of the inventive arc tube light source finishing process: filling. Once the body 22 is sufficiently flushed, the first needle valve 155a is closed, optionally a partial vacuum is drawn by the still-open evacuation line 153, and then the second needle valve 155b is opened to allow a fill gas to be passed through the second inlet 158b, into the chamber 162, through the holes 176 and/or slots 182 of the collet 174, and into the body 22, thereby filling the body 22 with the fill gas. Once a desired proportion of the flushing gas has been replaced by fill gas in the body 22, the body 22 is ready for a first seal. An advantageous feature of the inventive finishing head 150 is the small internal volume and small diameter of the chamber 162 plus inner tube assembly 172 plus necked-in portion 14. Especially when combined with a small volume bulb 18, the small internal volume becomes a pipeline that allows "slugs" of nearly unmixed gases to pass sequentially through, especially since the pipeline is also a small enough diameter to promote viscous flow rather than turbulent flow. Given suitable timing of the needle valves 155, it should be possible to position a slug of fill gas in the bulb 18 at the time that a first seal is effected in a bottom necked-in portion 14b (see Figure 10C), thereby minimizing the amount of expensive fill gas (e.g., Xenon) needed to fill the bulb 18.

Figures 10C and 15A illustrate a fifth step of the inventive arc tube light source finishing process: making a first seal 210a. Although Figure 10C adequately illustrates the act of sealing the body 22 about the foil 76, it should be apparent by comparison with Figure 15A that an illustration of arc tube sealing can be perfected by replacing the colletless bottom finishing head 151 with the colleted bottom finishing head 151', and by replacing the filament assembly 104 with the first and second electrode assemblies 302, 304. One further change is required in the case of making the first seal 210a when the collet 174 in the colleted bottom finishing head 151' is dimensioned such that the second electrode assembly 304 must be hanging from a spur 80 hooked over the collet 174 in order to attain a desired vertical positioning: in this case, the arc tube light source finishing stand 148' must be inverted 180 degrees to place the colleted bottom finishing head 151' on top during the making of the first seal 210a. The preferred sealing method, illustrated herein, is known as "shrink sealing", although the inventive light source finishing stand 148, 148' will accommodate other methods (e.g., pinch sealing). At a time when it is determined that the body 22 has been sufficiently flushed and is being filled with the fill gas,

a sealing burner 220 is applied to a bottom necked-in portion 14b of the body 22. For shrink sealing, the second needle valve 155 and/or the evacuation line valve 154 are adjusted to create a pressure within the body 22 that is near or slightly below ambient pressure, thereby assisting the shrink sealing. In Figure 10C, a top necked-in portion 14a illustrates the seal area before sealing, and the bottom necked-in portion 14b is shown at the completion of shrinking to form the first seal 210a. The size, shape, intensity, heating time, etc. for the sealing burner 220 and its flames are adjusted according to known methods for shrink sealing. Likewise, the sealing burner 220 may be oscillated for suitably applying heat around the perimeter of the bottom necked-in portion 14b. Uniform, even heating is needed in order to maintain axial alignment of the seal 210a and therefore of the electrode/foliated lead assemblies 302, 304 within. Preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around the foil 76 of a bottom foliated lead 74b to form a hermetic seal between the body 22 and the foil 76. Further preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around a bottom inner lead 82b to form an inner lead seal 212 for providing a desired bowl shape around and behind the electrode 306 or 308, and also for preventing stress at the transition from the bottom inner lead wire 82b to the foil 76. Further preferably, sufficient heat is applied such that the bottom necked-in portion 14b will shrink around a bottom outer lead wire 83b to form an outer lead seal 214 for preventing stress at the transition from the bottom outer lead wire 83b to the foil 76, and also for defining a preferred circular cross-section for the innermost portion of a bell mouth 216 that results from shrinking the innermost end of the bottom bugled end 16b. As will be seen in the description of light source mounting hereinbelow with reference to Figure 14, the bell mouth 216 does not have to be round, and furthermore can be quite shallow in depth, as long as there is room for an elbow 422 of an electrical support wire 416.

Figures 10D and 15A illustrate a sixth and final step of the inventive arc tube light source finishing process: making a second seal 210b (see Figure 15B for a view of the completed seal). Although Figure 10D adequately illustrates the act of sealing the body 22 about the foil 76, it should be apparent by comparison with Figure 15A that an illustration of arc tube sealing can be perfected by replacing the colletless bottom finishing head 151 with the colleted bottom finishing head 151', and by replacing the filament assembly 104 with the first and second electrode assemblies 302, 304. One further change is required in the case of making the second seal 210b when the collet 174 in the colleted bottom finishing head 151' is dimensioned such that the

second electrode assembly 304 must be hanging from a spur 80 hooked over the collet 174 in order to attain a desired vertical positioning: in this case, the arc tube light source finishing stand 148' was inverted for the first seal 210a, and must now be inverted 180 degrees again to place the collected bottom finishing head 151' back at the bottom during the making of the second seal

210b. After completion of the first seal 210a, a cooling nozzle 222 begins spraying a coolant 224 (e.g., liquid nitrogen) onto at least a lower portion of the bulb 18 of the body 22 in order to "freeze" a predetermined amount of the fill gas into the bulb 18. By closing the second needle valve 155b, freezing the fill gas will cause a below-ambient pressure within the body 22, thereby assisting in the shrink seal process. If desired, other solid or liquid phase arc tube light source ingredients (e.g., mercury and/or metal halide pellets) may also be dropped into the arc tube body 18 by known means (e.g., an inlet tube or passage, not shown, that opens into the inner tube 170). The sealing burner 220 is applied to the top necked-in portion 14a of the body 22. In Figure 10D, the top necked-in portion 14a illustrates the seal area before shrink sealing to form the second seal 210b (shown in Figure 15B). The second seal 210b is formed by a shrink sealing process as described hereinabove for the first seal 210a. After forming the second seal 210b, the coolant 224 and the various gas and vacuum lines can be turned off (valves closed); the sealing burner 220 can be extinguished and/or removed; and the clamshells 190 can be opened and the completed light source (in this case an arc tube 318) can be removed from the arc tube light source finishing stand 148'. Optionally a pilot flow of gas can be maintained in the chambers 162, 173' and in the outer tubes 168 as a means for releasing the seal to the bugled ends 16 and also as a means for preventing backflow contamination of the finishing heads 150, 151'.

Figure 15B shows a single view of the arc tube 318 finished according to the invention. It should be apparent that another view, rotated 90°, would appear the same except for the first and second seals 210a, 210b which would be viewed edgewise to the foils 76, as shown for a filament tube 218 in the view of Figure 10E. It should be understood that the scope of the invention includes light sources 218, 318 that have a first seal 210a that is rotated at a random angle relative to the second seal 210b. The first seal 210a and the essentially identical second seal 210b (collectively referred to as seals 210) are shrunk around the foils 76 of the first and second electrode assemblies 302, 304 to form hermetic seals between the body 22 and the foils 76. Preferably, the seals 210 are also shrunk around the inner leads 82 to form inner lead seals 212 for providing a desired bowl shape around and behind the electrode 306 or 308, and also for

preventing stress at the transition from inner lead wire 82 to foil 76. Further preferably, the seals 210 are also shrunk around the outer lead wires 83 to form outer lead seals 214 for preventing stress at the transition from outer lead wire 83 to foil 76, and also for forming bell mouths 216 having a preferred circular cross-section for the innermost portion of each bell mouth 216 that results from shrinking the innermost end of each bugled end 16. As will be seen in the description of light source mounting hereinbelow with reference to Figure 14, the bell mouth 216 does not have to be round, and furthermore can be quite shallow in depth, as long as there is room for an elbow 422 of an electrical support wire 416.

### **Lamp Assembly**

A feature of the present invention is that the inventive light sources (e.g., filament tubes 218 and arc tubes 318) can be simply and inexpensively mounted in a variety of lamp products, of which two embodiments are provided as examples hereinbelow. Many more configurations should become evident given the teaching of the present description.

Figure 13A shows a first of many possible exemplary embodiments of an inventive light source 450 (in this case, two filament tube light sources 218a, 218b) being mounted in a type of lamp that is a general service incandescent lamp 400. The incandescent lamp 400 has a transparent or translucent bulb/outer jacket 402 and an electrically conductive base 404 comprising an eyelet 406 and a screw-threaded shell 408. Fixed within the bulb 402 is a nonconductive stem 410 and a post 414 for supporting the two filament tube light sources 218a, 218b. A first filament tube light source 218a has a first outer lead wire 83a and an opposed second outer lead wire 83b, and a second filament tube light source 218b has a third outer lead wire 83c and an opposed fourth outer lead wire 83d. Electrical connections are provided for connecting the first and second filament tube light sources 218a, 218b in series, thereby forming a "Gemini Lamp". A first stem leadwire 412a (optionally including a fuse 407) is electrically and mechanically connected between the eyelet 406 and a first electrical support wire 416a that is nonconductively attached to the stem support post 414 (e.g., embedded in a glass bead on the post) and electrically and mechanically connected to the first outer lead wire 83a and to the first filament tube light source 218a by means of a first inventive electrical support connection 420a (further detailed hereinbelow with reference to Figure 14). A connecting electrical support wire 418 provides series electrical connection between the second outer lead wire 83b (on the first filament tube light source 218a) and the third outer lead wire 83c (on the second filament tube

light source 218b) by means of respective second and third electrical support connections 420b and 420c. Furthermore, the connecting electrical support wire 418 also helps provide support for the first and second filament tube light sources 218a, 218b by means of being attached to the stem support post 414 (e.g., embedded in a glass bead, or welded to a metallic stem support post 414). A second stem leadwire 412b is electrically and mechanically connected between the shell 408 and a second electrical support wire 416b that is nonconductively attached to the stem support post 414 and electrically and mechanically connected to the fourth outer lead wire 83d and to the second filament tube light source 218b by means of a fourth electrical support connection 420d.

Cost saving embodiments of the present invention that should be considered within its scope are envisioned wherein, for example, the stem support post 414 is eliminated and the first and second electrical support wires 416a, 416b are replaced by the first and second stem lead wires 412a, 412b, respectively, which are directly connected, electrically and mechanically, to the first and second filament tube light sources 218a, 218b by means of inventive electrical support connections 420. Known means of strengthening the first and second stem leadwires 412a, 412b and the connecting electrical support wire 418 should be adequate to support the two filament tube light sources 218a, 218b in a desired configuration under normal handling and operating conditions.

Figure 13B shows a second example of an inventive light source 450 (in this case, an arc tube light source 318) being mounted in a type of lamp that is a sealed beam headlamp 470. The sealed beam headlamp 470 has a reflector 472 and lens 473 and a pair of ferrules 474a, 474b located at the base of the reflector 472. The ferrules 474a, 474b are respectively connected to a pair of electrical terminals 478a, 478b. The arc tube light source 318 is both supported and electrically connected across the pair of ferrules 474a, 474b by first 482a and second 482b electrical support wires that are electrically and mechanically connected to first and second outer lead wires 83a and 83b, respectively. A first ferrule 474a is electrically and mechanically connected (e.g., by brazing) to the first electrical support wire 482a, which is in turn electrically and mechanically connected to the first outer lead wire 83a and to the arc tube light source 318 by means of a first inventive electrical support connection 420a. Similarly, a second ferrule 474b is electrically and mechanically connected to the second electrical support wire 482b, which is in turn electrically and mechanically connected to the second outer lead wire 83b and to the arc tube

light source 318 by means of a second inventive electrical support connection 420b. It may be noted that the electrical support wires 416, 418, 482 can have any desired cross-section, e.g., round, square, ribbon, etc.

Another feature of the present invention is an electrical support connection 420 (e.g., first, second, third, and fourth electrical support connections 420a, 420b, 420c, and 420d, respectively) that is enhanced by the flared-out bell mouth 216 and/or bugled end 16 on each end of the inventive light sources 218, 318 (e.g., filament tube light source 218 shown). Figure 14 shows a representative bell mouth 216 and bugled end 16 formed around an outer lead wire 83 that extends from an end of a light source 218. The bugled end 16 comprises an outward-opening cavity about the outer lead wire 83, and the cavity is optionally deepened as desired by the bell mouth 216. The electrical support connection 420 comprises an elbow 422 formed in an electrical support wire 416, 482 (e.g., 416 shown) such that the elbow 422 loops into the bugled end 16 of the bell mouth 216. The elbow 422 thus hooks the bugled end 16, thereby mechanically securing the light source 218, 318 given a holding force  $F_h$  that presses the elbow 422 into the bugled end 16. The holding force  $F_h$  may be provided by attaching the elbow 422 to the outer lead wire 83 (e.g., by welding), in which case the electrical support wire 416, 482 can end after the point of attachment (not shown). Preferably, the electrical support wire 416, 482 is formed in a loop 424 (e.g., the electrical support wire 416, 482 extends beyond the elbow 422 outward of the bugled end 16 and into a reverse-bent leg having a connection 426 (e.g., a crimped hook) that mechanically and preferably also electrically connects (provides an attachment of) the electrical support wire 416, 482 to the outer lead wire 83. Preferably the holding force  $F_h$  is applied to the loop 424 while the connection 426 is being made, thereby placing the outer lead wire 83 in tension for maintaining the holding force  $F_h$  and thereby assuring a secured light source 218, 318. Even without any significant magnitude of holding force  $F_h$ , simply hooking the elbow 422 within the bugled end 16 while connecting the electrical support wire 416, 482 to the outer lead wire 83 will provide a desirable stiffening of support for the light source 218, 318 as compared to the prior art. A further advantage of the inventive electrical support connection 420 is that it supports the light source (e.g., 218) by applying essentially lateral stresses on the relatively strong bugled end 16 but not on the outer lead wire 83, which only sees mostly longitudinal tensile stress. This is good because the wire-to-light source seal is relatively strong in tension but is subject to failure under lateral forces that tend to

bend the outer lead wire 83. It may be noted that the inventive electrical support connection 420 can be employed for mechanically supporting a light source (e.g., 218) while other means are used for electrically connecting the light source (e.g., 218).

### **Gemini Lamp**

5        The incandescent lamp 400 illustrated in Figure 13A is a preferred embodiment of a "Gemini Lamp", wherein the incandescent light source 450 within the outer jacket 402 comprises two halogen filament tubes 218a, 218b that are electrically connected in series, preferably with the filament tubes 218 mounted in a crossed configuration as shown (preferably crossing at an approximately 90° angle), thereby minimizing the amount of light from one filament tube (e.g., 10    218a) that is blocked by the other (e.g., 218b). Also preferably the outer jacket 402 is an inexpensive standard bulb of thin common glass (e.g., soda-lime glass with an average wall thickness of about 0.020"). Further preferably the outer jacket 402 is filled with an inexpensive dry inert gas (e.g., Nitrogen), or evacuated.

      There are many consumer advantages provided by the Gemini Lamp 400, and utilization  
15    of various inventive features disclosed herein are intended to significantly cost-reduce the Gemini Lamp 400 by providing means for mass production of inexpensive filament tubes 218 and means for their mounting in an outer jacket 402, thereby placing double-filament-tube general service lamps within a price range acceptable to household consumers. One of many advantages is a lamp efficacy improvement that is provided by the stretched-out leg 113 on either  
20    end of the coiled-coil filament 102. The stretched-out leg 113 design is more efficient than conventional coiled-coil filaments having single coil legs that consume some electrical power without producing any appreciable light. In general, the Gemini lamp utilizes every scrap of advantage to yield, in toto, a much more overall advantageous design.

      Significant safety advantages result from the inventive design. The Gemini lamp is a  
25    combination of two halogen lamps (e.g., filament tubes 218) in series, each one operating at half of the line voltage, and at half of the total lamp wattage. At the end of life in a halogen lamp, filament burnout generally produces a break in the cooler running end of the filament where failure occurs because of "notching". An arc can start, jumping the break in the filament, and then quickly spreading to an arc across the whole length of the filament, thereby heating the fill  
30    gas to high temperatures, enough to potentially explode the filament tube 218. The Gemini Lamp 400 has only half of the line voltage across each filament tube 218, thereby decreasing the

likelihood of arcing in the first place, and if it occurs anyway (e.g., in a first filament tube 218a), the still-burning series-connected second filament tube 218b will act like an arc tube ballast and will limit the arc current to a harmless level such that the arc cannot heat the fill gas enough to explode the failed first filament tube 218a. Further protection is provided by the stretched-out leg 113 of the filament 102 (see Figures 9B and 10F) that is positioned at the cooler ends of the filament 102 where the break generally occurs. Since the stretched-out leg 113 has very little mass, it burns back during arcing at a very high speed, and is lost to the arc when it burns into the inner lead seal 212. Decomposition products of vaporized quartz provide a cooling effect that tends to snuff out the arc as the wire of the filament leg 113 melts back into the quartz of the inner lead seal 212. This quenching of the arc appears to occur even faster than a fuse wire can melt in response to the arc. (Fuse wires are typically incorporated into one or both of the leadwires 412 where they pass through the base 404.) Even further protection is provided by using a filament tube body 22 having a very small diameter D1 of a circular cross-section, especially in the shrink sealed inner lead seal 212, all of which combine to provide an extraordinarily high burst strength. Side by side testing was conducted to compare failure mode of 100W, 120V Gemini Lamps 400 (with two series connected 50W, 60V halogen filament tubes 218a, 218b) versus lamps having the same outer jacket 402 but containing only one standard halogen filament tube (e.g., 1100) of the same total lamp operating voltage (120V) and wattage (100W). Failure was provoked by ramping up the lamp's line voltage until the tested lamp arced out. The conventional lamps 1170 all failed violently, wherein the arc exploded the quartz body (e.g., 1010). In contrast, the Gemini Lamps 400 all failed passively, wherein one of the two filament tubes 218 arced out, but did not explode.

The inventive lamp 400 provides significant cost savings when compared to prior art lamps (e.g., 1170 in Figure 1B). Gemini Lamp 400 components are fewer and cost less than components of comparable same-wattage quartz-halogen lamps. For example, the light source bulb 22 requires very little expensive quartz material, while the two filaments 104 combine to use almost the same length of tungsten wire of the same diameter, if not less length (due to the use of a more energy-efficient stretched-out leg 113 on a coiled coil filament 102). For example, the one piece foliated lead 74 efficiently uses a shorter length of smaller diameter molybdenum wire 42 and doesn't need foil that is inefficiently welded together in common three-part foliated leads. For example, the small volume light source body 22 uses less of an expensive fill gas



(e.g., Xenon), lesser still when the inventive finishing stand 148 and light source finishing process are employed. For example, the foliated leads 74 and the light source bodies 22 are efficiently mass-produced with virtually no waste. For example, expensive quartz cutoff saws are not needed to produce the bodies 22. For example, because of the safe failure mode of the Gemini Lamp 400, an inexpensive common outer jacket 402 can be used instead of "coke-bottle" enclosures with wall thicknesses approaching 0.250". For example, the stiffness of the stretched-out legs 113 and the shorter filament 104 (due to half the voltage and half the wattage) effectively shortens the unsupported span of the filament and reduces its sag and twisting, such that a smaller body diameter D1 can be employed, thereby reducing its cost. The half wattage filament also allows a smaller diameter body than a full wattage filament for the further reason that heat loading on the body is cut in half for the half wattage filament.

Although the invention has been illustrated and described in detail in the drawings and foregoing description, the same is to be considered as illustrative and not restrictive in character - it being understood that only preferred embodiments have been shown and described, and that all changes and modifications that come within the spirit of the invention are desired to be protected.

Undoubtedly, many other "variations" on the "themes" set forth hereinabove will occur to one having ordinary skill in the art to which the present invention most nearly pertains, and such variations are intended to be within the scope of the invention, as disclosed herein.